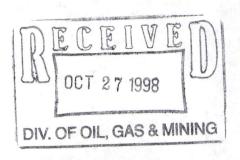


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# SF PHOSPHATES LIMITED COMPANY

# TAILINGS STORAGE FACILITY EXPANSION

PLAN OF OPERATIONS

July 24, 1998 Revised September 17, 1998

Prepared for:

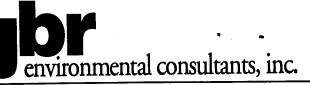
SF Phosphates Limited Company 9401 North Highway 91 Vernal, Utah 84078-7802

Submitted to:

Bureau of Land Management Vernal Field Office Vernal, Utah

Prepared by:

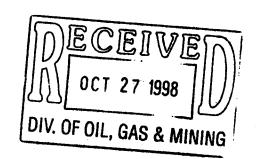
JBR Environmental Consultants, Inc. 8160 South Highland Drive Sandy, Utah 84093 (801) 943-4144



8160 South Highland Drive • Sandy, Utah 84093 • (801) 943-4144 • Fax (801) 942-1852

October 26, 1998

Mr. Tony Gallegos Division of Oil, Gas and Mining 1594 West North Temple Ste. 1210 Salt Lake City, Utah 84114



Re:

Tails Storage Facility Expansion, SF Phosphates LC, Vernal Phosphate Operation, M/047/007, Uintah County, Utah - Submittal of Revised Plan of Operations to the BLM

Dear Tony:

SF Phosphates Limited Company is proposing to expand the current tails storage facility to provide storage for tailings for an additional 40 years. JBR Environmental Consultants, Inc. was retained to assist their effort by producing the attached revised Plan of Operations (POO) for the Bureau of Land Management (BLM) Vernal Field Office. This version dated September 15, 1998 supersedes a previous POO that was submitted to your office.

On October 6, 1998, the BLM responded to SF Phosphates that this POO is sufficient to allow the Environmental Assessment process to begin. BLM requested that your office receive a copy and that any correspondence with them should make reference to the serial number assigned to the plan - UTU 76097. If you have any questions, please call Ron Ryan at (435) 781-3348 or me at (801) 943-4144.

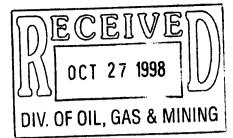
Sincerely,

Tim Thompson, P.E.

encl

cc Ron Ryan, SF Phosphates Peter Sokolosky, BLM

# SF PHOSPHATES LIMITED COMPANY TAILINGS STORAGE FACILITY EXPANSION PLAN OF OPERATIONS



# TABLE OF CONTENTS

INTRO	ODUCI	TION	1
1.0	APPI.	ICANT INFORMATION	1
1.0	1.A.	Claim Information	
	1.B	Individual Completing Application	
	1.C	Business Address and Telephone	
	1.C 1.D	Corporation Information	
		Authorized Field Representative Information	
	1.E.	Authorized Field Representative information	2
2.0	CURR	RENT OPERATIONS	
	2.A.	Location and Project Area Disturbance	2
	2.B.	Mining Operations	3
	2.C.	Processing Operations	
	2.D.	Tailings Storage Facility (TSF)	
		2.D.a Current TSF Permits Issued by Other Agencies	
	2.E	Tailings Solids Characteristics	5
	2.F.	Tailings Water Characteristics	
	2.G.	Geology	
	2.H.	Geohydrology	3
	2.II. 2.I.	Ancillary Facilities	
	2.1.	Anchary Pacifics	. •
3.0	PLAN	OF OPERATIONS - TSF EXPANSION 1	6
	3.A.	Proposed Project Area	16
	3.B.	Proposed Tailings Dam Raise	7
	3.C.	Proposed Inundation Area	7
	3.D.	Hazardous Materials Management	8
	3.E.	Other Regulatory Permit Activities	8
4.0	RECL	AMATION PLAN 1	
	4.A.	Statement of Reclamation Activities	20
	4.B.	Reclamation Schedule	21
	4.C.	Post-Mining Land Use	22
	4.D.	Post-Mining Topography	22
	4.E.	Potential Reclamation Issues	22
		4.E.a Nutrient Status	
		4.E.b Salt Accumulation	
		4.E.c Wind Erosion	
		4.E.d Molybdenum	
		4.E.e Arid Climate	25
		T.L.C And Chinate	

	4.F.	Revegetation	25
		4.F.a Current Nutrient Status of Tailings	25
		4.F.b Site Specific Revegetation Procedures	26
		4.F.c Reclamation Seed Sources	
		4.F.d Potential Revegetation Species	
		4.F.e Slimes Nurse Crop Species	
		4.F.f Slimes Final Crop Species	
		4.F.g Sand Beach and Spillway Pool Species	
		4.F.h Potential Amendments	
		4.F.i Final Seedbed Preparation	
		4.F.j Seeding	
	4.G.	Interim Reclamation and Test Plots	
	4.H.	Post Reclamation Maintenance and Monitoring	
5.0	STAT	EMENT OF RECLAMATION AND CLOSURE RESPONSIBILITY	31
6.0	RECL	AMATION COSTS	31
7.0	PUBL	IC SAFETY	31
8.0	BIBLI	OGRAPHY	33
		LIST OF FIGURES	
		EIST OF TIGURES	
Figure	1	Location Map	
Figure		Tailings Storage Facility Map	
Figure		Geology Map	
Figure		Tailings Dam Cross Section	
1 iguit	7	Tannigs Dan Cross Section	
		LIST OF APPENDICES	
		DIST OF ATTEMPTOES	
Apper	ndix A	Mill Site Claims Summary	
Apper	ndix B	Reclamation Tables from Golder Associates, May, 1998 Table 7. Nutrient Applyage Laboratory Popults	
		Table 7 - Nutrient Analyses Laboratory Results	
		Table 8 - Acid-Base Accounting Results	
		Table 9 - Potential Reclamation Species Slimes Nurse Crop	
		Table 10- Potential Reclamation Species Final Cover - Slimes  Table 11 Potential Reclamation Species Sand Species	
		Table 11- Potential Reclamation Species - Sand Species	
		Table 12- Potential Reclamation Species - Pond Area	
		Table 13- Qualitative Descriptors of Soil Surface Status	
A	din C	Water Rights	
Apper	ndix C	water Rights	

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# PLAN OF OPERATIONS FOR THE SF PHOSPHATES LIMITED COMPANY TAILINGS STORAGE FACILITY

SF Phosphates Limited Company (SF Phosphates) operates a phosphate mining and milling operation north of Vernal, Utah. Phosphate slurry is then transported by a 96-mile pipeline to a fertilizer processing plant located near Rock Springs, Wyoming. The projected life of the mine is on the order of 100 years. Preparation of the phosphate ore at the mine site results in the production of tailings which are currently stored in a facility specifically designed for this purpose. The mining and processing operation employs approximately 125 people.

This Plan of Operations (POO) is for the expansion of the existing Tailings Storage Facility (TSF). It is being submitted in compliance with the BLM regulations for mining operations on public lands under the general mining law (43 CFR 3809). SF Phosphates has patented claims on the land where the existing 365 acre TSF is located. This proposed expansion of the TSF will encompass approximately 184 acres. This expansion acreage includes 23.8 acres of BLM administered land along the south property line which will be impacted by the proposed raise of the existing tailings dam and subsequent inundation with tails. Mill site claims, totaling 63.4 acres, have been filed to cover that impacted area.

An expansion of the TSF is necessary because it is estimated that the current facility will be filled to maximum capacity by the year 2006. Since the anticipated life of the mining operation extends well beyond this, additional tailings storage capacity must be developed. Expansion will occur as seven 15 to 18 ft. lifts spread over the next 35 to 40 years. Continued construction on the existing dam will allow phosphate production to continue with minimal impact to the environment. At the currently planned production rates, the proposed raise design would provide enough tailings capacity for about 44 more years of operation. Tailings storage at the "B" site or other remote areas may be needed in the distant future.

#### 1.0 APPLICANT INFORMATION

#### 1.A. Claim Information

SF Phosphates has filed a block of Mill Site claims located in Sections 5 & 6,T.3 S., R.22 E and Section 1, T.3 S., R.21 E. These claims total 63.4 acres and are located on federal land administered by the Vernal Field Office of the Bureau of Land Management (BLM). In Appendix A, a table titled "Mining Claims Summary" shows the mill site claim names and the BLM serial numbers.

# 1.B Individual Completing Application

This Plan of Operations is submitted by M.A. Weaver, Mine Manager on behalf of SF Phosphates.

# 1.C Business Address and Telephone

The business address for SF Phosphates is:

SF Phosphates Limited 9401 North Highway 191 Vernal, Utah 84078 Telephone: (435) 781-3348 Fax: (435) 789-2944.

# 1.D Corporation Information

The property was initially developed by the San Francisco Chemical Company in 1958. It was purchased by Stauffer Chemical Company in 1968 and then by Chevron Resources Company in 1981. In April, 1992, the mine, pipeline, and fertilizer plant were purchased by J.R. Simplot Company, a privately held agribusiness company in Boise, Idaho, and Farmland Industries, Inc., an agricultural food marketing and manufacturing cooperative in Kansas City, Missouri. SF Phosphates Limited Company was formed as an independent company through this joint venture.

# 1.E. Authorized Field Representative Information

The authorized field representative and daily contact is Ron Ryan at the address and phone number listed above.

# 2.0 CURRENT OPERATIONS

# 2.A. Location and Project Area Disturbance

The location of the existing SF Phosphates mine and concentrate production plant is approximately 11 miles north of Vernal, Uintah County, Utah (Figure 1, Location Map). This Plan of Operations is for the portion of the expansion of the existing SF Phosphates TSF onto public land administered by the BLM. The existing TSF is located adjacent to the SF Phosphates concentrator (Figure 2, Tailings Storage Facility Map). The permitted area of the current TSF is 365 acres. The legal location of this feature is:

NE/4, SW/4 SE/4, Section 36, T. 2 S., R. 21 E. NW/4, NE/4, Section 1, T. 3 S., R. 21 E. SE/4, SW/4, Section 31, T. 2 S., R. 22 E. NE/4, NW/4, Section 6, T. 3 S., R. 22 E. SW/4, Section 32. T.2 S., R. 22 E. NW/4, Section 5, T. 3 S., R. 22 E.

The entire property covers an area of approximately 23 square miles on the south slope of the Uintah Mountains in northeast Utah. The elevation of the property is approximately 6,000 feet. Access to the property is via Highway 191 which bisects the property. The perennial Big Brush Creek flows through the property immediately north of the concentrator in a deep gorge and leaves the property east of the tailings dam. Prominent nearby features include Red Fleet Reservoir on Big Brush Creek approximately 2 miles east of the property boundary; Steinaker Reservoir approximately 4 miles south; and Ashley National Forest immediately north and west of the property.

# 2.B. Mining Operations

Approximately 3.8 million tons of phosphate ore are mined annually at the mine. Topsoil is removed from the area to be mined and is placed on previously mined areas which have been prepared for reclamation or it is stored until such areas are ready to receive topsoil. Following the removal of topsoil, overburden is blasted to loosen the material. This overburden material is then relocated to mined-out areas. Once the overburden is removed and the ore is exposed, the ore is blasted and loaded into trucks using shovels or front-end loaders. The ore is then trucked to a portable crusher and conveyor where it is crushed to minus 10 inches and then transported to a 110,000 ton surge pile. Conveyors then transport this product to a semi-autogenous grinding (SAG) mill. The ground ore slurry from the SAG mill is then pumped through a 1.5 mile long pipeline to the concentrator facility (mill).

# 2.C. Processing Operations

At the mill, the ore slurry is ground further in a ball mill in closed circuit with hydrocyclone classifiers. Clay fines from the classifiers are considered tailings and are pumped to the TSF. The coarser material from the classifiers is conditioned in mixer tanks with flotation reagents including: diesel oil, fatty acid, and polymers and then processed through a bank of flotation cells. In the flotation cells the phosphate mineral grains are separated from the barren sand which is pumped to the TSF tailings dam cyclones. The phosphate mineral grains are removed from the top of the flotation cells and pumped to a thickener where the density of the slurry is adjusted before being pumped through a 95-mile long slurry pipeline to a fertilizer plant in Rock Springs, Wyoming. Clarified water from the TSF is reclaimed in a barge-mounted pump and returned to the grinding facility for reuse.

# 2.D. Tailings Storage Facility (TSF)

The Tailings Storage Facility (TSF) includes the both dam(s) and the impoundment of water and tailings. Two types of tailings slurry produced in the mill are transported separately to the TSF for disposal. Fine tailings slimes are discharged by gravity flow to the northeast area of the tailings impoundment. Coarser tailings from the flotation cells are typically pumped to the crest of the tailings dam, are cycloned there and discharged along the upstream face of the dam. The sand fraction of the cycloned tailings solids forms a 150 to 200-foot wide sand beach along the upstream face of the dam and the clay and silt slimes fraction flow to the western portions of the

SF PHOSPHATES SEPTEMBER 17, 1998
PLAN OF OPERATIONS, PAGE 3

impoundment. Ultimately, all of the tailings will be discharged over the extended embankment. Clarified tailings water is reclaimed from the west end of the impoundment at a barge-mounted reclaim pump to be recycled to the mill process. The supernatant pond covers much of the tailings surface. It is shallow over most of the tailings and attains its maximum depth in the western area of the impoundment near the reclaim barge. Water reclaimed from the TSF is reused in the grinding process. It is also used for transporting the phosphate concentrate to Rock Springs in the slurry pipeline.

When the concentrator first commenced operations in 1961, tailings slurry from the concentrator was piped to a tailings storage impoundment located behind a dam built of waste rock to an elevation of about 5915 feet in an ephemeral drainage immediately south of the concentrator. The first tailings storage facility was known as Tailings Pond No.1. In 1973 the capacity of the tailings storage was increased by construction of Tailings Dam No.2 which crossed two ephemeral drainages immediately south of Tailings Pond No.1. The initial Tailings Dam No.2 was built from mine waste rock to an elevation of approximately 5880 feet but was subsequently raised with three upstream lifts to a maximum elevation of 5,900 feet.

In 1985, Morrison-Knudsen Engineers, Inc. completed a final design for a major expansion of the TSF by raising the tailings dam (M-K, 1985). Beginning in 1986, both of the earlier tailings dams were covered with an earthfill dam that produced the combined tailings storage facility (TSF) that exists today. This dam was constructed in a downstream manner over both of the previous dams using soils and Moenkopi Formation rock borrowed from within the impoundment area.

The current dam crest is at an elevation of approximately 5952 feet and is planned to be raised to a final crest elevation of 5,970 feet in 2000 when its maximum height will be 268 feet. The downstream slope of the current tailings dam is approximately 2.5h:1v and its top width is approximately 140 feet. The overall length of the current dam is approximately 5,600 feet and the area of the tailings impoundment is approximately 326 acres. A 10-foot freeboard is maintained above the maximum elevation of the tailings at the upstream face of the tailings. At the current rate of tailings discharge, the capacity of the currently approved TSF will be consumed in about 2006. Therefore, additional tailings capacity will be necessary through raising the elevation of the tailings dam.

The existing tailings dam is constructed of compacted siltstone obtained from local borrow areas in the Moenkopi Formation. Seepage of tailings water through the dam is controlled with chimney drains, blanket drains, and collector drains that intercept seepage and direct it to the downstream toe of the dam. The downstream outlets of the three main collector drains are fitted with measuring devices to allow the seepage flow rates to be individually monitored. These outlets are located at the downstream toe of the dam in the bottoms of three main drainages crossed by the dam.

# 2.D.a Current TSF Permits Issued by Other Agencies

Permits to operate the current tailings storage facility are being obtained and/or updated as part of this expansion proposal. No permits are required by the EPA or Utah Division of Solid and

Hazardous Waste. The Utah Division of Water Quality has assigned Case File # UGW 47001 to process the Ground Water Discharge permit that has been submitted to their office. Issuance is expected in 6-12 months. The Utah Division of Water Rights, Dam Safety, has assigned Permit # UT00814 to the expansion of the TSF for the life of the facility. They have reviewed the design and amendments are currently being prepared. The previous dam application has Permit # UT00410. The Utah Division of Oil, Gas and Mining approved the Mining Reclamation Plan for the mine and TSF on September 5, 1980, permit # M/047/007, valid for the life of the mine. It allows SF Phosphates to deposit and store tailings from their beneficiation operations behind an earthen embankment. Copies of applications for permits and approved permits can be provided.

# 2.E Tailings Solids Characteristics

The chemical and mineralogic composition of the tailings solids is inert, non-hazardous and stable. Characteristics of the future tailings can be expected to be very similar to those which are being experienced in the current operations. Tailings are generally fine to very fine grain sediment mineral particles with very low concentrations of heavy metals or acid producing materials. These characteristics signify that this proposed facility is not likely to adversely impact human health or the environment.

Based on information collected by SF Phosphates from samples of tailings obtained in 1991 and 1996, the tailings solids are expected to have the physical characteristics described below:

Slurry Density	50	Percent Solids
Maximum Grain Size	40	Mesh
Minus 200 Mesh Solids	90.5	Percent
Pyrite		1-2 Percent
Quartz		25-37 Percent
Carbonates	22-27	Percent
Clays		12-15 Percent
Ca-Apatite	27-30	Percent

The tailings deposited in the TSF are ground ore and water with small quantities of flotation reagents. The only source of waste entering the TSF is the SF Phosphates concentrator tailings.

Approximately 2,447,000 tons of ground ore are disposed of in the tailings pond annually. The fine tailings are low plasticity clay and silt with 95 - 100 % passing the No.200 sieve (Knight Piesold, 1997). The sand tailings are a silty sand with less than 20% passing the No. 200 sieve. The dry density of the tailings solids ranges from about 80 to 112 pcf. Various analyses have been conducted of the tailings solids between 1982 and 1997. These analyses indicate that the tailings are non-toxic, non-acid-forming, similar to natural soils in their chemical characteristics, and are not a significant potential source of ground water pollution. The specific analytical results for each sampling event are presented in the following narrative and tables.

SF PHOSPHATES SEPTEMBER 17, 1998
PLAN OF OPERATIONS, PAGE 5

In 1982, Chevron obtained 3 samples of tailings for EP Toxicity Tests. Results of these analyses are shown in Table 2-1. This is the latest available data and has been included in the ground water permit application to the Utah Division of Water Quality. These data show that the tailings had very low concentrations of all the Resource Conservation and Recovery Act (RCRA) toxic metals as well as low concentrations of antimony, cobalt, manganese, nickel and zinc.

Table 2-1 1982 EP Toxicity Results for Tailings Solids (mg/l)

Constituent	Reg. Level*	Sample #1	Sample #2	Sample #3
Arsenic	5.0	<.001	.016	.003
Antimony	None	<.001	<.001	<.001
Barium	100.0	.965	1.450	.899
Cadmium	1.0	.004	.002	.007
Chromium	5.0	.020	.005	.012
Cobalt	None	<.001	<.001	<.001
Lead	5.0	.133	.095	.006
Manganese	None	.005	.065	.025
Mercury	0.2	.0003	.0002	.0010
Selenium	1.0	.005	.002	<.001
Silver	5.0	.005	.004	<.001
Nickel	None	.015	.017	.055
Zinc	None	.445	.669	.775

<sup>\*</sup>Regulatory Level - from Table 1 "Maximum Concentration of Contaminates for Toxicity Characteristics (40CFR 261.24)

In 1991, S F Phosphates sampled the tailings solids and the tailings water in a number of locations. The tailings solids were analyzed for pH, TCLP and total metals. The analytical results for the 1991 tailings solids metals analyses are shown in Table 2-2. These results indicate that the metal concentrations in the tailings are within the range typically found in soils of the western United States (EPA, 1986)

Table 2-2 1991 Total Metals Results for Tailings Solids (mg/kg)

Parameter	SE-1	SE-2	SE-3	SE-4	SE-5	SE-6	SE-7	SE-8	Normal*
pН	7.8	7.8	7.5	7.6	7.2	7.2	7.5	7.3	
Phosphate	12.8	16.1	15.9	1.7	18.5	13.5	12.1	10.4	
Sulfate	137	285	1720	5860	482	2740	303	8140	
Fluoride	5.8	5.6	5.4	2.1	1.8	9.6	21.6	2.7	
Silver	<1.0	1.1	<1.0	1.8	<1.0	<1.0	<1.0	<1.0	
Arsenic	12.1	10.8	7.5	<1.0	2.7	8.1	11.1	8.6	6
Barium	358	279	197	77.3	152	152	265	135	580
Beryllium	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	
Cadmium	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	0.06
Chromium	693	866	431	14.1	11.4	13.4	482	53.4	100
Copper	10.1	6.6	5.4	3.8	13.1	10.4	8.9	9.6	20
Mercury	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25	.083
Nickel	35.9	30.8	21.0	3.7	10.9	11.1	29.7	17.4	40
Lead	6.1	6.0	3.7	3.0	6.5	10.6	5.9	6.4	10
Antimony	<3.0	<3.0	<3.0	<3.0	<3.0	<3.0	<3.0	<3.0	
Selenium	3.7	5.3	2.6	<1.0	<1.0	<1.0	2.9	<1.0	0.5
Thorium	<1.0	<2.0	1.9	<1.0	<1.0	<1.0	<1.0	<1.0	
Zinc	96.7	83.4	52.6	15.1	36.3	36	88.5	50.0	50

<sup>\*</sup> Common concentration in soil materials in Western U.S. (EPA, 1986)

Samples of tailings solids were analyzed for TCLP parameters in 1991. These results are shown in Table 2-3 and indicate that the tailings did not exceed any of the regulatory levels for the RCRA hazardous toxicity waste characteristics.

Table 2-3 1991 TCLP Results for Tailings Solids (mg/l)

table 25 1991 Telli Results for Tamings Bonds (mg)								
Parameter	SE-I	SE-2	SE-7	SE-9	Reg. Level			
Arsenic	<0.01	<0.01	<0.01	<0.01	5.0			
Barium	0.44	0.38	0.48	0.51	100			
Cadmium	<0.005	<0.005	<0.005	<0.005	1.0			
Chromium	<0.01	0.03	0.01	0.01	5.0			
Lead	<0.03	<0.03	<0.03	<0.03	<0.03			
Mercury	<0.005	<0.005	<0.005	<0.005	0.2			
Selenium	0.06	<0.03	0.04	0.05	1.0			
Silver	<0.01	<0.01	<0.01	<0.01	5.0			
Pesticides	ND		ND	ND	Varies			
Semi-Vols	ND		ND	ND	Varies			
Volatiles	ND	ND	ND	ND	Varies			

<sup>\*</sup>Regulatory Level - from Table 1 "Maximum Concentration of Contaminates for Toxicity Characteristics (40CFR 261.24)

In 1997 Golder Associates analyzed samples of tailings solids for use as plant growth medium. These results are shown in Table 2-4. These data indicate that the tailings solids have neutral pH, are not saline, and do not exhibit levels of soluble metals that will be phytotoxic. They are deficient in some plant nutrients.

Table 2-4 1997 Plant Nutrients Results for Tailings Solids

Parameter	Sand I	Sand 2	Sand 3	Slime 1	Sime 2	Sime 3	Catucal Value
pН	7.2	7.0	7.1	7.2	7.2	7.2	<5.0 or >8.5
EC	1.79	2.63	2.20	2.65	2.71	2.62	<8
SAR	0.38	0.31	0.14	0.43	0.46	0.44	>10
Phosphate	3.80	2.54	2.20	14.8	12.5	13.5	<7
Potassium	94.0	87.0	68.0	82.0	84.0	82.0	<120
Nitrate	1.24	1.04	0.92	0.74	0.50	0.48	<10
Copper	0.24	0.34	0.32	0.46	0.46	0.46	None
Lead	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	None

Parameter	Sand 1	Said 2	Sand 3	Slime I	Slime 2	Slime 3	Critical Value
Arsenic	0.44	0.36	0.21	0.45	0.44	0.46	None
Boron	0.17	0.24	0.13	0.20	0.22	0.23	<0.5 or >5
Selenium	0.02	0.02	<0.02	0.02	0.02	0.02	>0.1
Molybdenum	0.66	0.71	0.73	0.66	0.63	0.71	0.5 - 1.0
Zinc	0.46	1.48	5.10	0.64	0.60	0.62	<1.0

<sup>†</sup> Values above which phytotoxicity may occur and below which deficiencies may result.

Golder Associates also analyzed samples of tailings sands and slimes for acid-base accounting testing in 1997. The results of these tests is shown in Table 2-5. These data show that the tailings are not acid generating and are strongly neutralizing.

Table 2-5 1997 Acid-Base Accounting Results for Tailings Solids

Sample	Carbonate (percent)	Total Sulfur (percent)	Acid Potential (/1000)*	Neut.Potential (t/1000t)*	Acid-Base Potential (Neut Pot-Acid Pot.)
Sand 1	12.4	0.93	29.1	127	98.0
Sand 2	12.1	1.89	59.0	125	65.5
Sand 3	12.2	1.73	54.0	128	73.6
Slime 1	13.8	1.22	38.1	136	97.5
Slime 2	13.9	1.17	36.6	142	106
Slime 3	13.7	1.21	37.8	106	98.8

<sup>\*</sup>Tons of calcium carbonate per 1000 tons of material.

# 2.F. Tailings Water Characteristics

Samples of tailings water were obtained and analyzed in 1991 and 1996. These analyses indicated that the tailings water met all ground water standards and drinking water standards with the exception of TDS and sulfate which were above the secondary drinking water standards. The specific analytical results for each sampling event are presented in the following narrative and tables.

This is the latest available data and has been included in the ground water permit application to the Utah Division of Water Quality. The Ground Water Standards shown in the tables below were adopted by the Utah Department of Environmental Quality as maximum contaminate levels for the protection of ground water quality. The frequency of future sampling and analysis of the tailings water will be determined when the permit is approved.

<sup>\*</sup> Elemental results are in ppm plant available (soluble) concentrations.

Tailings water samples were analyzed in 1991 for total metals, TDS, EC, P, SO<sub>4</sub>, and F. The results of the tailings water analyses are shown in Table 2-6. These results indicate that the tailings water met all Utah Ground Water Standards under R317-6-2 for metals. It was slightly above the standard for fluoride in one sample (SW-2, 5.1 mg/l) but the average fluoride concentration for the samples was within the standard.

Table 2-6 1991 Analytical Results for Tailings Water (mg/l)

Parameter	SW-2	SW-3	SW-5	SW-7	G.W.Standare
pН	7.86	7.88	7.87	7.84	6.5 - 8.5
EC	1130	1150	1190	1250	NS
Phosphate	1.60	0.14	0.07	0.17	NS
Sulfate	1390	1260	1560	1400	NS
Fluoride	5.1	3.3	3.4	3.2	4.0
TDS	1670	1760	1700	1730	NS
Antimony	<0.03	<0.03	<0.03	<0.03	0.006*
Arsenic	0.004	0.003	0.002	0.003	0.05
Barium	0.05	0.05	0.05	0.07	2.0
Beryllium	<0.005	<0.005	<0.005	<0.005	0.004*
Cadmium	<0.005	<0.005	<0.005	<0.005	0.005
Chromium	<0.01	<0.01	<0.01	0.02	0.1
Copper	<0.02	<0.02	<0.02	<0.02	1.3
Lead	<0.002	<0.002	<0.002	<0.002	0.015
Mercury	<0.0005	<0.0005	<0.0005	<0.0005	0.002
Nickel	0.05	0.05	0.04	0.05	0.1*
Selenium	0.003	0.003	0.003	0.002	0.05
Silver	<0.01	<0.01	<0.01	<0.01	0.1
Thallium	<0.002	<0.002	<0.002	<0.002	0.002*
Zinc	0.03	0.04	0.02	0.06	5.0

<sup>\*</sup> Not listed in R317-6-2 (Admin. Rules for ground water quality protection) but are EPA Maximum Contam Levels

In 1996 SF Phosphates analyzed a grab sample of tailings water for full-spectrum chemistry. The

results of these analyses are shown in Table 2-7. The results of these analyses indicate that none of the analyses exceeded primary drinking water standards. Both TDS and sulfate exceeded the secondary drinking water standards. Iron and phosphorous slightly exceeded the water quality standard for Big Brush Creek (Class 3A).

Table 2-7 1996 Results for Tailings Water (mg/l)

Parameter	Result	Primary Drinking Water Standard	Secondary Drinking Water Standard	Utah Surface* Water Standard
pН	7.6	6.5-8.5	NS	6.5-9.0
EC	2380	NS	NS	NS
Alkalinity	112	NS	NS	NS
Ammonia	0.07	NS	NS	19.5
Bicarbonate	112	NS	NS	NS
BOD (5 day)	1	NS	NS	5
Carbonate	<2	NS	NS	NS
Chloride	12	NS	250	NS
Cyanide	<0.01	0.02	NS	0.022
Fluoride	<1.0	4.0	2.0	NS
Gross Alpha	14 pCi/l	15 pCi/l	NS	15 pCi/l
Gross Beta	25 pCi/l	Man-made only	NS	50 pCi/l
Hardness	1480	NS	NS	NS
Nitrate as N	< 0.02	10.0	NS	4
Nitrate/Nitrite	< 0.02	10.0	NS	NS
Oil & Grease	<2	NS	NS	NS
Phosphorus	0.070	NS	NS	0.05
Sulfate	1480	NS	250	NS
TDS	2230	NS	500	NS
Arsenic (total)	0.003	0.05	NS	- 0.36
Barium (total)	0.022	2.0	NS	NS
Calcium (diss.)	405	NS	NS	NS

Parameter	Result	Primary Drinking Water Standard	Secondary Drinking Water Standard	Utali Surface* Water Standard
Chromium (tot)	< 0.02	0.1	NS	1.7
Iron (dissolved)	0.03	NS	0.3	0.02
Iron (total)	0.06	NS	NS	NS
Magnesium (d)	113	NS	NS	NS
Selenium (total)	0.003	0.05	NS	0.02
Sodium (diss)	41.2	NS	NS	NS
Zinc (total)	0.04	NS	5.0	0.12
Volatiles (624)	ND	Varies	NS	NS

<sup>\*</sup> Class 3A (Ground water which is protected as a potential source of drinking water, after substantial treatment, and as a source of water for industry and agriculture).

# 2.G. Geology

The TSF is located on the south flank of the Uinta Mountains where erosion has deeply incised south-dipping sedimentary rocks of Triassic and Permian age. Big Brush Creek, the nearest perennial surface water body to the TSF, flows through Big Brush Creek Gorge to the north of the TSF and passes within 2000 feet to the east of the existing dam. The proposed TSF lift will be constructed by up-stream methods and will not result in the TSF being closer to Big Brush Creek than it is at the present time.

The rocks in the TSF vicinity have been uplifted and gently folded by the uplift of the Uinta Arch to the north and by southeast striking secondary folds which form two sub-parallel southeast striking and plunging anticlines near the TSF. The uplift of the Uinta Arch has resulted in the sedimentary rocks beneath and adjacent to the TSF having an 8 to 10 degree dip to the south.

The surficial bedrock geology in the vicinity of the TSF is shown on Figure 3, Geology Map. The south and south-southeast dip of the sedimentary rocks in the area have resulted in younger rocks being exposed to the south of the TSF and older rocks exposed to the north. The bedrock formations exposed in the project vicinity range from the Pennsylvanian Weber Quartzite to the Triassic Moenkopi Formation. In addition, the Morgan Formation, which underlies the Weber Quartzite, while not exposed in the project vicinity, has been intercepted by deep water supply wells drilled by SF Phosphates and its predecessors. The upper Morgan Formation consists of interbedded sandstone, limestone and shale. The total thicknesses of the Morgan in the project vicinity is believed to be 1000 to 1400 feet.

The Weber Quartzite ranges in thickness from 1015 to 1275 feet and is comprised of medium-grained, cross-bedded sandstone and massively bedded, fine-grained quartzose sandstone. This formation is exposed north of the TSF, especially in deeper canyons and gorges.

The Permian Park City Formation overlies the Weber Quartzite. This formation ranges in thickness from 140 to 150 feet in the vicinity of the TSF and is comprised of two members: the basal phosphatic member which is comprised of 24 to 28 feet of hard, cherty, phosphatic mudstone with minor sandstone; and the overlying upper Park City Formation which is 110 to 130 feet in thickness and is made up of cherty and sandy dolomitic limestone interbedded with shale and fine-grained sandstone (Hood, 1976).

The Triassic Moenkopi Formation consists of a thin-bedded siltstone, fine-grained sandstone, and sandy shale and ranges from 820 feet to 1120 feet in thickness. Gypsum can be common in the Moenkopi and results in highly gypsiferous zones within the formation. The lower Moenkopi forms the bedrock beneath the TSF where it consists of thin-bedded, reddish brown siltstone and fine-grained sandstone with thin partings of weak, red, sandy shale and thin beds of light greenish-gray fine-grained sandstone (Golder, 1998).

Overlying the Moenkopi and cropping out to the south of the TSF are the Shinarump Conglomerate, a thin (1 to 60 feet thick) medium to coarse-grained sandstone with quartzite pebbles, and the Chinle Formation (approximately 260 feet thick) which is comprised of red, variegated shale in the lower two-thirds of the unit and sandstone with thin red shale interbeds in the upper one third of the formation.

The axis of a north-northwest-striking, south-plunging, low-amplitude anticline has been mapped a short distance to the north of the TSF. The absence of detailed geologic mapping in the Moenkopi prior to initial tailings deposition and the absence of sufficiently deep drill holes to the west, south or east of the TSF to identify correlative stratigraphic horizons make it difficult to determine that this fold is present in the Moenkopi beneath the TSF. No faults have been mapped or otherwise identified beneath or in the vicinity of the TSF (Figure 3). A northwest striking fault is believed to be coincident with Big Brush Creek Gorge north of the TSF; however, this fault would not intercept the TSF and if it does extend to the south, would lie several thousand feet east of the TSF dam.

# 2.H. Geohydrology

The geohydrologic properties of the formations in the TSF vicinity have been described by Dames and Moore (1974), International Engineering Company (1982), and Hood (1976). In addition, Golder (1998) has measured the permeability in the Moenkopi Formation in the vicinity of the TSF. Ratliff Spring is shown on Figure 2, Tailings Storage Facility Map.

The Weber Quartzite is the principal aquifer in the project vicinity. SF Phosphates currently obtains water for its mill and product transport pipeline from six deep wells completed in the Weber. A total of nine wells have been completed in this aquifer by SF Phosphates and its predecessors; many of

SF PHOSPHATES
PLAN OF OPERATIONS,

SEPTEMBER 17, 1998 PAGE 13 these wells are not in service. According to Dames and Moore, the Weber Quartzite is comprised of an upper cross-bedded section approximately 300 to 400 feet thick underlain by massively bedded, well cemented quartzite ranging in thickness from approximately 700 to 800 feet. The unit is highly fractured with vertical fractures spaced 10 to 30 feet apart and continuous for "...several tens to hundreds of feet." This assessment was based on examination of the unit in outcrop in Big Brush Creek Gorge and in an observation well drilled in support of a pump test of well DW-B. Although primary, intergranular permeability is significant in the Weber, most of the permeability, as determined by geophysical logging of selected wells by Dames and Moore, is secondary in the form of fractures. Aquifer test data by Dames and Moore, re-analyzed by Hood, resulted in calculated transmissivity of 2,700 square feet per day. Much of the storativity in this unit exists in the upper more uncemented, cross-bedded section. Dames and Moore determined that:

"Although the artesian inflow into Well [DW]-A is mainly from fractures, these are not necessarily the prime water yielding zones under pumping conditions. During pumping, the intergranular permeability of the sandstone undoubtedly accounts for a dominant portion of the well yield."

Ground water in the Weber Quartzite is confined under artesian conditions and the potentiometric surfaces observed in wells that have been completed in the Weber Quartzite represent head conditions in the lower Weber Quartzite or possibly the underlying Morgan Formation. The aquitard or confining layer for the Weber is not described in the literature; however, it is presumably the basal mudstone member of the Park City Formation, possibly combined with a low primary-permeability zone at the top of the Weber Quartzite. The potentiometric gradient is south to southeast. The Morgan Formation, which is comprised of interbedded sandstone and limestone, is penetrated by 4 of the 9 water supply wells and, based on the results of geophysical logging performed under the direction of Dames and Moore, yields water under artesian conditions to well DW-A.

The potentiometric surfaces reflect the effects of pumping of the wells for water supply purposes. Several of the wells were reported to have encountered artesian or near artesian conditions at the time of drilling. Table 2-8 is a summary of potentiometric data from the water supply wells for which data are available. The down-dip-most wells, WW-A and WW-E, both encountered artesian conditions, as would be predicted given the greater depth of the confined unit and the resulting increased head. Well WW-E and the TSF are located in approximately the same positions relative to the to the dip of the bedrock; therefore, similar depths to the Weber Quartzite and potentiometric heads within that unit would be expected beneath the TSF as have been observed in Well WW-E. The resulting upward hydraulic gradient in the Weber Quartzite and the presence of the intervening aquiclude should effectively prevent infiltration of the confined aquifer by any tailings water that may be released from the TSF.

Table 2-8 Artesian and Potentiometric Data from Water Supply Wells Completed in the Weber Ouartzite

	Weber Quartzite		
Well	Wellhead Elevation (Feet AMSL)	Head at Completion (Feet AMSL)	Potentiometric Surface After Pumping (Feet AMSL)
WW-A	5712	Artesian; head unknown	5421 to 5247
WW-B	5976	5974 to 5975	5908 to 5834
WW-C	6172	No Data	No Data
WW-D	6124	No Data	5917
WW-E	5712	Artesian; head unknown	5706
WW-H	6080	No Data	5863
WW-I	6083	5896	No pump installed

The Park City Formation is a potential aquifer in the area and Hood (1974) reports, where the contains fractures that have been enlarged by solution of the limestone beds, the yields can be large. Drilling in the project vicinity has not encountered significant quantities of water in this formation; however, the potential for aquifer development down dip to the south exists if it receives recharge, perhaps from the underlying Weber Quartzite. The potential for impacts of the TSF on the Park City Formation is low given the presence of the relatively low-permeability Moenkopi Formation between the base of the TSF and the Park City Formation.

The Moenkopi Formation is not a water supply aquifer and any water production from the Moenkopi would be of very low yield and poor quality. The results of packer tests by IECO in 1982 showed permeability ranges from 0 in unfractured bedrock to  $3.3 \times 10^{-5}$ cm/sec where the bedrock is fractured. The southward dip of bedrock in the TSF area could make it possible for migration of water from the TSF down dip to the south, if fracturing in the Moenkopi is sufficiently extensive. If the anticlinal axis that has been mapped to the north of the TSF extends beneath the site of the TSF and has folded the Moenkopi, tension fracturing near the anticlinal axis could be present.

Quaternary alluvium adjacent to creeks in the area can serve as an aquifer and yield flow to shallow wells (Hood, 1976). Ground water is produced from alluvium adjacent to Big Brush Creek east of the TSF in a shallow well owned by SF Phosphates and located near the guard shack at the entrance to the facility. Permeability information on this aquifer is not available.

IECO identified a thick layer of residuum above the Moenkopi bedrock in the area beneath the TSF (see detailed discussion in section 7.0). An upper low permeability zone of sandy silt reportedly overlies a more permeable gravely, silty sand just above the contact with the Moenkopi bedrock.

The lower gravely sand could provide a conduit for flow of infiltrating water down hill topographically in a general west to east direction. This subsurface flow could reach the alluvial aquifer associated with Big Brush Creek in the vicinity of the meadow east of the TSF.

The Weber Quartzite and all of the younger formations exposed in the project area are subject to direct recharge from precipitation as the result of their exposure along the flanks of the Uinta Arch. Because the Park City Formation has low primary porosity and is partially eroded over much of the area, recharge from precipitation is probably insignificant. Dames and Moore reported that several small springs on the SF Phosphates property discharge from the lower limestone of the Park City and postulate that these springs are recharged by the underlying Weber Quartzite or deeper formations. The demonstration by Dames and Moore (1974) that artesian discharge from a fracture zone within the Morgan Formation to well WW-B lends further support to the concept of recharge of the Weber Quartzite aquifer by underlying, older units. Godfrey (1985) presented a strong argument for the recharge of springs in the Weber Quartzite from much older carbonate units exposed to the east where karst development provides pathways for recharge. He also demonstrated that trans-basinal flow through karst solution channels is common in the incised canyons north of the TSF.

A substantial amount of the base flow in Big Brush Creek and Little Brush Creek (to the east of Big Brush Creek) apparently arises from discharge as springs from the Weber Quartzite either directly or from the lower limestone of the Park City Formation via solution channels developed along fractures (Maxwell, et. al., 1971). This spring discharge along with the discharge contribution from precipitation within the Big Brush Creek watershed is the probable source of recharge to the shallow alluvial aquifer east of the TSF.

# 2.I. Ancillary Facilities

Ancillary facilities located at the SF Phosphates mine operations include offices, warehouses, and shop complex. These facilities provide administrative, logistical, and maintenance functions necessary to the operations. Additional facilities used to transport the phosphate slurry from the mine to a processing plant located in Rock Springs, Wyoming, include a pumping system at the plant site with three 2000 horsepower pumps to pump the phosphate slurry through the 96-mile pipeline.

#### 3.0 PLAN OF OPERATIONS - TSF EXPANSION

#### 3.A. Proposed Project Area

The TSF is located on the south flank of the Uinta Mountains where erosion has deeply incised south-dipping sedimentary rocks of Triassic and Permian age. Big Brush Creek, the nearest perennial surface water body to the TSF, flows through Big Brush Creek Gorge to the north of the TSF and passes within 2000 feet to the east of the existing dam. The proposed TSF lift will be constructed by up-stream methods and will not result in the TSF being closer to Big Brush Creek than it is at the present time (see Figure 2, Tailings Storage Facility Map). Red Fleet Reservoir State Park is located approximately two miles east-southeast from the TSF.

SF PHOSPHATES
PLAN OF OPERATIONS,

# 3.B. Proposed Tailings Dam Raise

A design for the proposed modifications to the TSF has been prepared by Golder Associates (Golder, 1998). The existing tailings dam will be raised sequentially using an upstream construction method from the existing crest elevation of 5952 feet to 6060 feet, a total raise of 108 feet. Construction raises or lifts will occur approximately every 5 to 7 years until maximum dam height is reached. The first raise of 18 feet will finish the existing dam to its design crest elevation of 5970 feet. Six additional raises, each 15 feet in height, are proposed to follow. The last raise will encroach upon approximately 0.05 acres of a mill site claim on BLM land. The overall downstream slope would remain at 2.5h:1v and crest width would vary from the current 140 feet to 50 feet at the 6060-foot elevation (Figure 4, Tailings Dam Cross Section).

The raised dam is expected to be constructed with on-site Moenkopi siltstone material from a ridge within the proposed impoundment area (see Figure 2). This borrow fill will mined in a conventional manner primarily using scrapers, dozers, end loaders, shovels and trucks. Some blasting and ripping will be required. Material will be salvaged from the lowest elevations first in advance of the rising water/tails. It is estimated that over 3 million cubic yards of material will be needed. Although pit depths could reach 50 feet, no adverse effects on ground water are expected in the nearly 1,000' thick Moenkopi. Other borrow sources have been reviewed and are not considered favorable at this time.

In the area of these proposed borrow operations, the surface is owned by SF Phosphates. This ridge, which is in the west half of T.2S., R.22E., Sec.31, has reservations of some minerals (oil, gas and phosphate) to the Federal Government. Borrow material taken from this area for the proposed expansion of the TSF would not be expected to be subject to a mineral material sale. Any phosphate which may exist below this borrow area is very unlikely to be of any commercial value as determined in the past by SF Phosphates. Hence, this area was and is being utilized for tailings storage. Should borrow pit design or field exploration change the proposed borrow area, the BLM will be notified.

Seepage control in the proposed raise would be provided by the 150 to 200-foot wide cycloned sand beach deposited along the upstream face of the dam. This permeable sand zone would direct seepage downward to the internal drain system of the existing dam. This drain system would continue to function as in the past, directing the seepage to the three collector drains in the same three locations as the current operations.

At the currently planned production rates, the proposed raise design would provide enough tailings capacity for about 44 more years of operation.

# 3.C. Proposed Inundation Area

The proposed expansion of the TSF will encompass approximately 184 acres; 160 acres on SF Phosphates' property and 23.8 acres on the Mill Sites filed on public land. This is the maximum acreage which would be covered with tails or water during the operating life of the facility. As shown on Figure 2, Tailings Storage Facility Map, the proposed final inundation level is expected to reach just over the 6050 foot elevation.

After thirty-some years of operation, water will first begin to encroach upon the public lands as whole tails fill the lower elevations of the impoundment. After forty-some years the tails will replace the water along the south property line. For final reclamation, grading and redistribution of the tailings will done. The highest elevation of tailings will be at the dam (eastern side) at approximately 6057 ft. The spillway discharge channel on the north side will be at an elevation of about 6053 ft. Thus it is calculated that a pool of runoff water could form in the center of the impoundment on SF Phosphates' property. However, water is not expected to accumulate on the public lands to the south. The final disposition of the surface of BLM lands will be dry tails reclaimed as described in Chapter 4. The final tailings surface on the southern edge of the impoundment would be a vertical distance of about 100 feet up from the existing tailings surface. The final tailings surface would also be at least 100 feet below the ridge line.

At this time, there are no roads within this very rugged public lands area and none are planned. In the future, a discharge pipeline from the mill could possibly be situated on the southern end of the tailings dam area. Currently there is a Utah Power & Light electric transmission line which crosses the tailings pond near the eastern side of Section 6. Studies are in progress to determine the required modifications to span the pond. It is possible that fewer support towers would be used for the transmission line and that only towers on SF Phosphates' property will be affected.. The relocation plan anticipates using the existing right-of-way and the grantee is not expected to relinquish their prior existing rights.

# 3.D. Hazardous Materials Management

No deleterious materials or wastes will be produced by these operations. Less than 10,000 pounds of any chemical(s) from EPA's Consolidated list of Chemicals Subject to Reporting Under Title III of the Superfund Amendments and Reauthorization Act (SARA) of 1986, and less the Threshold Planning Quantity (TPQ) of any extremely hazardous substance(s), as defined in 40 CFR 355, will be used, produced, transported, stored, disposed, or associated with the proposed operation. Vehicle and equipment fuel, lubricants, antifreeze and battery acid will be the only hazardous materials used or associated with the proposed notice level work. Risk of a release will be minimal because it would be cleaned up immediately and disposed of in approved manner.

# 3.E. Other Regulatory Permit Activities

The mill site claims for 35 acres south of SF Phosphates' property are included in the Red Mountain-Dry Fork Area of Critical Environmental Concern (ACEC). This complex was designated by the Vernal Field Office of the Bureau of Land Management (BLM) in the Diamond Mountain Resource Area (DMRA) Resource Management Plan and Record of Decision, (RMP/ROD)(BLM, 1994), Decision SEA01. Expansion of the TSF would occur below the ridgeline of Red Mountain on its north slope and would not be noticeable from the ACEC except from the top of the mountain looking down on all of SF Phosphates existing operations.

SF PHOSPHATES
PLAN OF OPERATIONS.

A further decision of the DMRA RMP/ROD, RD 32, establishes a Special Recreation Management Area (SRMA) to cover the ACEC complex. The Red Mountain Potential Recreation Area is listed within Level 2, Careful Management, which allows activities that do not detract from the resource values being protected.

There are some sensitive resources within the ACEC, in addition to recreational values. These include raptor nesting habitat, deer and elk winter habitat and visual resources. Cultural resources have been evaluated within the mill site claims, and there were no eligible sites located within the area to be inundated by the tailings. Also, there are no threatened, endangered, or sensitive plant issues known in the mill site claims area. Issues of this nature will be addressed as part of the Environmental Assessment process.

The Division of Oil, Gas and Mining has been apprised of these expansion plans and will be forwarded a copy of this POO for their review and comment. They currently hold the mining reclamation bond and will regulate additional bonding requirements as needed.

An application for a Ground Water Discharge Permit has been submitted to the Utah Division of Water Quality. Responses to that agencies' comments are currently being prepared.

The Division of Water Rights - Dam Safety is also reviewing the engineering specifications and drawings associated with this project. Responses to that agencies' comments are also currently being prepared.

The Division of Air Quality is reviewing an initial operating permit application for a Title V permit. Issuance is expected in early August, 1998.

#### 4.0 RECLAMATION PLAN

The reclamation plan for the future closure of the TSF will incorporate direct seeding of the tailings solids. The proposed final revegetation program would include seeding a crop of grass directly into the tailings solids as soon as the water drains off and they can be accessed for seeding.

The outer slopes of the tailings dam will be seeded as necessary during the life of the TSF to reduce erosion of the slope. It is expected that this slope will be adequately revegetated at the end of the TSF operations and will not need to be further reclaimed.

A tailings sampling program was conducted in 1997 and Golder Associates reviewed the potential for the dried tailings sand and slimes to support a perennial vegetative cover (Golder, 1998). Direct seeding of the tailings solids is a very viable approach to reclamation based upon the following characteristics. The tailings analyses indicated that the tailings pH is neutral. No soluble metals were identified at concentrations which would result in plant phytotoxicity. Soluble salts activity was at acceptable concentrations and acid-base accounting results indicated the tailings are strongly

SF PHOSPHATES
PLAN OF OPERATIONS,

SEPTEMBER 17, 1998

neutralizing and will not become acidic. There were deficiencies of available boron, zinc, nitrogen, potassium, and organic matter.

The reclamation requirements of the Division of Oil, Gas and Mining and the Bureau of Land Management will be followed in the final closure of the TSF. The final closure requirements of the Utah State Engineer, Dam Safety Office, will be followed for drainage and monitoring of the impoundment and dam.

#### 4.A. Statement of Reclamation Activities

SF Phosphates proposes to increase the authorized surface disturbances from 365 acres to approximately 548.5 acres. However, only 23.8 acres of this disturbance will occur on lands administered by the BLM. Most of this new disturbance will result from inundation of lands by impounded tailings.

It is the intention of SF Phosphates to reclaim this proposed expansion of the Tailings Storage Facility (TSF) to meet all federal and state requirements. Reclamation will be both concurrent, to the extent practical, and post use, following plans described herein. The reclamation approach and procedures outlined in this section were developed for the site-specific conditions of this area. The procedures are designed such that the disturbance areas are reclaimed to a productive use similar to the pre-mining land uses, and the reclaimed areas are visually and functionally compatible with the surrounding topography.

The conceptual reclamation plan described in this section has been prepared primarily by Golder Associates to provide the general framework for reclamation of the TSF. Given the long duration of this mining operation, SF Phosphates recognizes that the "state of the art" in reclamation may change significantly by the time the TSF is ready for reclamation. Also, changes in the beneficiation process and/or ore may result in a final tailings surface with different physical and chemical characteristics from those which currently exist. The methods and concepts presented in this section will likely be reevaluated and revised over the life of the project. Therefore, this plan will concentrate on identifying potential issues that may be encountered in reclaiming the tailings, and how these issues will be addressed.

This plan presents the current condition of the tailings, discusses potential issues related to closure, stabilization and revegetation of the TSF, and presents conceptual methods to accomplish closure. The preferred closure method must stabilize the tailings surface, provide a viable post-closure land use, be technically and economically feasible, and allow permanent "walk-away" closure. Three possible closure options were initially considered:

- \* wet cover
- , soil cover
- \* direct revegetation

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A wet cover would be difficult to maintain in the semi-arid climate conditions at the project. Net evaporation would require the artificial addition of water to maintain a wet cover. This would preclude "walk-away" closure. Therefore, a wet cover was not considered practical.

A soil cover is also not an option because soil resources in the project vicinity are sparse and poorly developed. Soil recovery operations would be extremely difficult because of the large natural variations in topography. At a minimum soil cover of 2 inches, approximately 161,000 cubic yards of soil would be required to cover the tailings surface at closure. Soil would need to be borrowed from undisturbed areas in the project vicinity, creating a large additional area of disturbance, or else would need to be imported from outside the project area. No soil sources in the area have been identified. Importing soil is considered logistically and economically unfeasible.

Direct revegetation is the most realistic alternative since soil properties of the tailings suggest that they are a good topsoil substitute. Currently, volunteer vegetation has been growing in areas where tailings have been exposed. Direct revegetation of phosphate tailings has also been successfully performed in the eastern U.S. The specific amendment requirements are a function of many factors. Therefore, an integral component of this plan is to develop reclamation techniques based on knowledge gained prior to closure through the evaluation of test plots constructed on-site.

The goal of reclamation is to return the tailings to a condition that is compatible with the proposed post-mining land uses of wildlife grazing and watershed protection. Specific goals are to:

- \* provide a stable surface which resists water and wind erosion
- \* provide wildlife habitat
- \* promote establishment of a stable vegetative community
- \* protect surface water and groundwater quality

Successful direct revegetation of the tailings surface can accomplish these goals.

#### 4.B. Reclamation Schedule

The proposed TSF expansion will allow operations to continue through the year 2042. Reclamation activities will be performed concurrently, to the extent practical, and immediately after the operation ceases. An exact schedule is not possible to determine at this time since there will be many years of operational decisions which will affect such timing.

Final vegetation of the downstream face of the tailings dam will begin as soon as construction of each raise is completed. The timing of this activity will be adjusted so that seeding will take place during either the spring or late fall planting seasons to maximize probability of vegetative success. Revegetation of the tailings surface will occur when surface conditions permit and at the end of the useful life of the facility.

Test plots will also be established in order to gain experience in direct revegetation of the tailings surface. These plots are further described in Section 4.G.

#### 4.C. **Post-Mining Land Use**

The proposed post-mining land use for the TSF expansion will be wildlife grazing and watershed protection.

#### 4.D. **Post-Mining Topography**

During the final years of operation of the TSF, the tailings discharge points will be adjusted as necessary to produce a final grade on the tailings solids toward the north end of the tailings dam where a spillway channel will be excavated. This channel will be designed to comply with Utah State Engineer requirements and to drain the peak flow from the PMP falling in the watershed above the tailings dam. This channel will prevent any significant accumulation of meteoric water against the tailings embankment.

The outer slope of the tailings dam will be constructed at a 2.5h: 1v overall slope and has been shown to be stable under static and dynamic conditions (Knight Piesold, 1997, Golder, 1998). Therefore, the outer slope of the tailings dam will not be regraded at the end of operations of the TSF. The revegetated face of the embankment will minimize erosion. By the end of operations, the upstream slope of the dam will almost be covered with a beach of tailings sand so the upstream slope of the dam will also not require regrading.

Reclamation of the proposed TSF will result in an area with less relief than the pre-mining topography for the area where tailings are deposited. The average grade of the reclaimed tailings surface will be on the order of about 0.5%. The reduced relief will result in several benefits to the area. The reclaimed site will experience less erosion and greater water retention resulting in improved vegetation for use by wildlife.

#### 4.E. **Potential Reclamation Issues**

Several factors that are often the major concerns during reclamation of metal mines are not anticipated to be a problem for the SF Phosphates tailings. These include pH, which is neutral; metals, none of which were at phytotoxic levels; salts, which occur at acceptable levels; and, acid generation, which is not predicted to occur based on the strong acid neutralizing characteristics of the tailings. Many of the remaining issues are representative of the background conditions in the 1-NOT SPECIFICALLY
PECATED TO TAILINGS area and are not specifically related to the tailings. The factors which may complicate revegetation of the tailings are:

GAVICATERIALS N. P. K and O.M. deficiency

- \* potential salt accumulation over time (upward migration of soluble salts)
- \* wind erosion

- \* molybdenosis toxicity to animals
- arid climate
- \* available water holding capacity
- \* surface crusting

Past experience with older tailings disposal areas at the site has shown that natural revegetation occurs quite readily on the tailings surface. Therefore, it can be concluded that none of the factors listed above will likely prohibit successful reclamation of the tailings with direct revegetation techniques. Each of these factors, and how they can be addressed during a carefully planned and executed reclamation process, are discussed below.

# 4.E.a Nutrient Status

The tailings are currently not an ideal growth medium due to low concentrations of plant available N, P, K and low O.M. Little topsoil occurs in the area and so supplementation by topsoil borrow material is not likely to be an option.

Nitrogen's primary function is to encourage above-ground vegetative growth and regulate utilization of potassium and phosphorus. Phosphorus serves many functions in the development of plants. A few of the most important include:

- \* cell division
- \* flowering and fruiting
- , plant maturation
- root development
- disease resistance

Of these, the most important is generally root development. Potassium is essential for photosynthesis, chlorophyll formation, disease resistance, and seed formation, as well (Brady 1974). O.M. affects plant germination and survival more indirectly through the modification of soil properties. O.M. improves veil 'properties by improving infiltration and moisture holding capacity, encouraging aggregation, buffering soil temperature, and increasing cation exchange capacity. O.M. is also necessary for the development of mycorrhizal roots (Harvey 1982) which are necessary for the survival of many plant species. O.M. has been demonstrated to be essential to revegetation of phosphate-mined lands (Brumwell and Carrier 1989).

As previously stated, topsoil in the area is poorly developed and scarce. Therefore, the proposed approach to stabilization of the tailings is to directly revegetate the tailings using ameliorative and adaptive procedures. Direct revegetation will be supplemented by the selective redistribution of salvaged soil, if available.

The ameliorative approach involves chemically altering the soils to correct factors which may limit plant growth. Based on soil analysis, a site-specific combination and application rate of low-cost waste materials and standard reclamation amendments are specified to accomplish the required soil

modification. Major nutrient deficiencies can also be addressed by adding fertilizers to the amelioration mixture.

The adaptive approach involves identifying, specifying, and establishing plants that are ecotypically differentiated, or adapted and tolerant of, the site conditions. Laboratory plant tolerance testing methods can be used to rapidly and cost-effectively screen a large number of plants for their tolerance to the specific conditions found at the site. This method involves using Agar (a gelatinous growth medium) and growth media adjusted chemically to emulate the specific site conditions. Since a plant's germination and initial root growth response are indicative of its response to actual site conditions, species that are adapted to site conditions can be rapidly evaluated and selected.

#### 4.E.b Salt Accumulation

Soluble salts of sodium, calcium and magnesium are currently not available in concentrations which could limit plant growth. However, the tailings are currently inundated. During and following closure, the ponded water will be removed and the tailings will dry out. Arid regions are characterized by excessive surface evaporation and soluble salts may accumulate in the surface horizon. Given the fine texture of the slimes, the potential exists for accumulation of salts and formation of saline conditions. If a salt accumulation hazard is identified, salt tolerant species will be selected for use in the reclamation seed mix. However, the local Natural Resource Conservation Service (NRCS) office indicates that no saline soils have been identified in the vicinity of the project and it is not anticipated that salt tolerant species will be necessary.

#### 4.E.c Wind Erosion

The texture of the tailings surface is predominantly silt-sized particles. Silts are highly susceptible to wind and water erosion. The relatively gentle slope at closure should minimize water erosion concerns. However, wind erosion will be a concern as the surface dries out. Methods to control wind erosion include physical barriers to slow and break up wind velocity, surface roughening, and covering the soil surface with a synthetic sealant, organic matter, and/or coarse fragments. However, the most proven, efficient and cost effective method to control wind erosion is to rapidly establish vegetation on the surface.

#### 4.E.d Molybdenum

Molybdenosis is a disease which affects ruminants, particularly cattle and sheep, and can result in mortality. To date, no molybdenosis has been observed. Although none is expected, a monitoring program will continue. Since no livestock grazing is proposed for the closed TSF, there will be no risk to cattle and sheep. Deer and elk are also affected, but to a lesser degree than cattle and sheep. The disease is due to copper deficiency caused by a complex and poorly understood reaction between copper, molybdenum and sulfur. Generally, when molybdenum and sulfur levels are elevated and copper levels are low, molybdenosis may occur. Cu:Mo ratios in plant tissues of less than 2:1 have been shown to cause molybdenosis unless dietary copper levels exceed 13 to 16 ppm. Unfortunately, molybdenum uptake levels are difficult to predict and not well correlated to concentrations in soil. In addition, some species, particularly legumes, can accumulate molybdenum at concentrations well above soil concentrations. The laboratory analyses indicate the plant available Cu:Mo ratio in the

SF PHOSPHATES
PLAN OF OPERATIONS,

tailings is currently less than 1:1. The tailings analyses indicated total molybdenum concentrations of 5 to 6 ppm. Barchad (1948) reported molybdenosis in soils with total molybdenum concentrations of 1.5-5.0 ppm. Therefore, test plots will be constructed to include collecting and analyzing plants - ALPOADY STATED THIS EXCLUSION for copper and molybdenum levels in plant tissues. If, laboratory analyses indicate Cu: Mo ratios in plant tissues are less than 2:1, several options are available. They include:

\* choosing species which do not accumulate Mo

, managing the TSF to exclude cattle following closure

using a fertilizer amendment that includes chelated copper to increase plant available

\* copper

# 4.E.e Arid Climate

There has been no evidence of surface crusting on any of the older tailings at the site and none is anticipated. However, the arid climate and fine texture of the tailings could potentially result in the formation of a crust on the surface. If a crust were to form, it may act as a barrier to infiltration and further reduce available moisture for plants. The crust may also inhibit plant emergence following germination. Addition of organic amendments and mulch increase soil moisture and encourage the formation of stable soil aggregates which will minimize crusting and increase infiltration and plant available moisture.

#### 4.F. Revegetation

# 4.F.a Current Nutrient Status of Tailings

The tailings impoundment currently covers approximately 326 acres. At closure the TSF will cover approximately 600 acres. Currently, the surface of the tailings includes a 200-foot wide beach area composed of loamy sands up gradient of the tailings embankment beach area. The remainder of the tailings contain slimes which have a silt loam texture. The slimes are currently saturated and covered by standing water. Six tailings samples (three sand and three slimes) were collected in January 1998 and analyzed for texture, nutrient status, plant available and total metals, and acid-base accounting. The results are presented in Tables 7 and 8 (Appendix B).

Laboratory results were reviewed to identify the potential for metal-induced toxicity or potential nutrient deficiencies. The analyses were compared to soil suitability criteria determined by reviewing published data from various sources. It should be noted that the criteria presented in Table 7 are guidelines only as there is considerable variation in the available literature. Actual effects of a given metal concentration will vary as a function of many factors, including plant species, soil pH, climate, and redox potential.

The laboratory results indicate the tailings are currently deficient in plant available nitrogen(N), potassium (K) and organic matter (O.M.). Cation exchange capacity is low due to the low percentage of clay and organic matter. The sandy loam tailings are deficient in phosphorus (P). The relative lack of plant available P in the sandy loam tailings may be explained by the X-ray diffraction (XRD) results, which indicate the dominant phosphate mineral is apatite, a calcium-phosphate

SF PHOSPHATES PLAN OF OPERATIONS, SEPTEMBER 17, 1998 PAGE 25

mineral which binds phosphorous in insoluble (unavailable) forms. This deficiency is further complicated by the lack of organic matter, which would tend to increase the availability of phosphorus. Tailings pH (saturated paste) is neutral. No metals were identified at concentrations which could result in plant phytotoxicity. Plant available boron and zinc are at concentrations which could result in deficiencies. Molybdenum is present at slightly elevated concentrations. Soluble salts activity is currently at acceptable concentrations. Acid-base accounting (ABA) results (Table 8) indicate the tailings are strongly acid neutralizing.

# 4.F.b Site Specific Revegetation Procedures

At closure, the majority of the tailings surface will consist of slimes in a saturated condition. It is anticipated that it will take a number of years before the slimes have consolidated and drained to the point where reclamation equipment can operate on the surface. Therefore, as soon as an area is drained of standing water, a nurse crop of seed, fertilizer, mulch and tackifier will be sprayed or aerially-applied (by airplane or helicopter). An alternative, which will be investigated during the mine life, is to hydraulically apply amendments and fertilizer by mixing it into the final stages of tailings deposition. The fertilizer and mulch rates will be determined based on nutrient analysis of samples collected near the end of the mine life and information gained through revegetation test plots performed during operations.

#### 4.F.c Reclamation Seed Sources

Reclamation species mixtures will be developed for each area prior to closure. The species and application rates will be determined based on results of test plots and nutrient testing of the tailings prior to reclamation. If available at the time of reclamation, seed will be purchased from commercial suppliers. Seed will be developed from stocks that are adapted to the moisture regime and elevation of the site. If desired species are not commercially available, commercial suppliers can collect seed from adapted plants and produce the necessary quantity of seed if given a 2- to 3-year lead time. Ideally, parent stock should be collected from the project area. If sufficient sources are not available near the project, seed sources will be collected from sites with similar elevation and moisture regimes. Woody species will be planted as bare-root or containerized seedlings.

# 4.F.d Potential Revegetation Species

Tables 9 through 12 (Appendix B) present potential species for inclusion in the final seed mix. The four lists include potential species for the following areas/stages:

- \* slimes nurse crop
- \* slimes final crop
- sand beach
- \* spillway pool

# 4.F.e Slimes Nurse Crop Species

The slime nurse crop species were selected based on their tolerance to silt and clay textures and average annual precipitation of 15 inches or greater, corresponding to the period immediately following the end of tailings deposition when the tailings will still be wet. The slimes nurse crop

will be seeded, probably by aerial means, as soon as standing water no longer remains in the impoundment. It's purpose is to provide immediate stabilization of the tailings surface, and to promote natural succession by increasing evapotranspiration and imparting shade and organic matter to the tailings. It will also protect the surface from wind and water erosion and provide protected micro sites for more desirable species to establish. The nurse crop seed mix will consist of a mixture of species which will establish in the current mesic moisture regime, but will not persist as the tailings dry to a more xeric condition typical of the surrounding area.

# 4.F.f Slimes Final Crop Species

The slimes final crop species were selected based on their tolerance to silt and clay textures and annual precipitation of 13 inches or less, corresponding to long-term, post-closure conditions. The extent to which seeding with the final crop species is required will depend on the degree of natural succession that occurs on the tailings during the drying and consolidation period. Unless acceptable vegetation species adapted to the anticipated long-term conditions become established relatively quickly through natural succession, seeding with the final slimes species mix will need to be performed to ensure permanent vegetation survival.

# 4.F.g Sand Beach and Spillway Pool Species

The sand beach species were selected based on their tolerance to sandy textures and annual precipitation of 13 inches or less. The spillway pool species were selected based on their tolerance to standing water or riparian areas. These species have all been identified as native to the area or having commercially available cultivators adapted to site conditions.

# 4.F.h Potential Amendments

When the tailings have dried to the point where they can support heavy equipment, the nurse crop will be tilled in and the tailings will be seeded with a seed mixture consisting of species selected from the test plots. Fertilizer and other amendment rates will be determined based on the nutrient status of the tailings at the time of seeding and test plot results.

Based on the current nutrient status of the tailings, the following fertilizer and amendments would be required to sustain a permanent vegetation cover:

Sands	<u>Slimes</u>
60 pounds P <sub>2</sub> O <sub>5</sub> /acre	None
40 pounds K <sub>2</sub> O /acre	40 pounds K <sub>2</sub> O /acre
40 pounds N/acre	40 pounds N/acre
10 tons O.M./acre	10 tons O.M./acre

These recommendations are based on the tailings laboratory data discussed earlier. Specific amendment recommendations will be developed prior to reclamation and be based on results of test plots and nutrient analysis performed immediately prior to reclamation. The O.M. recommendation is based on the assumption that the current O.M. content is negligible. Although the laboratory results indicate about 1 percent O.M., iron is known to interfere with the laboratory analysis resulting

SF PHOSPHATES
PLAN OF OPERATIONS,

SEPTEMBER 17, 1998

in positive errors (Lee 1939). The laboratory results indicate significant concentrations of iron. The O.M. amendment rate has been formulated to raise the O.M. level by approximately 1 percent. O.M. sources may include:

- sewage sludge
- \* hay or straw
- , manure
- \* sawdust or sawmill scraps
- \* commercial organic fertilizers, such as Biosol
- \* nurse crop/green manure

A nurse crop is the most effective and cost-efficient technique to add O.M. to the tailings and help to ensure long-term survival of the permanent vegetation mix. The proposed nurse crop presented in Section 9.4 will provide a portion of the required O.M. Test plots during the mine life will determine the suitability of nurse crop species and the amount of soil O.M. contributed by the nurse crop. The final O.M. application rate will be determined to provide a rate comparable to natural soils in the area.

The ratio of carbon to nitrogen in the soil affects the rate of organic matter breakdown and nitrogen availability. As a general rule, at a C:N ratio of about 20:1 or less there is usually a net release of mineral nitrogen. At higher ratios, decomposition of organic material is slowed and nitrogen is used by soil microorganisms to decompose O.M., making the nitrogen unavailable to plants. Therefore, the final nitrogen fertilization rate will depend on the amount and type of O.M. added, since various O.M. materials have widely differing C:N ratios.

Phosphorus, K and O.M. should be added to the soil and, if possible, incorporated at least one month prior to seeding to allow P and K to contact the root zone and decomposition of the O.M. to begin prior to seeding. Excess fertilization with inorganic nitrogen will encourage establishment of weedy species which compete with the desired species. Therefore, nitrogen should be added in the spring following a fall seeding to reduce competition during initial establishment.

# 4.F.i Final Seedbed Preparation

Once the tailings surface has dried enough to be trafficked by agricultural equipment, the seedbed should be prepared by ripping with a chisel plow or similar implement to a depth of approximately 6 inches. This step may be eliminated, modified, or restricted to certain areas of the TSF if significant permanent-type vegetation has already become established on the tailings as a result of earlier aerial or hydraulic seeding efforts and natural succession. Ripping loosens the soil surface and reduces resistance to seedling emergence and root growth. It also provides a roughened surface which reduces wind and water erosion and provides protected micro-sites for seedling establishment.

# 4.F.j Seeding

Seeding and planting should be planned for early fall to take advantage of winter and spring precipitation. Exposed beaches will be sprayed each spring with the specified hydro mulch. Seed

SF PHOSPHATES
PLAN OF OPERATIONS.

may be broadcast or drill-seeded. Drill seeding places the seed to a specified depth and covers it with soil. Broadcast seeding scatters the seed on the surface. Seeds are broadcast by dry methods or wet methods using a hydro seeder. Dry methods include centrifugal broadcasters, blowers or aircraft. Drill seeding is generally considered the superior method for arid and semi-arid sites. It assures that seed is distributed uniformly, at the proper rate and covered to the proper depth for germination. The drill seeder allows placement of different size seeds at the appropriate depth. One disadvantage of drill seeding is that the seeds are planted in straight rows resulting in a less natural appearance than for broadcast seeding. If broadcast seeding is used the seed is susceptible to predation by birds and small mammals, loss from wind, and some seeds may not adequately contact the soil.

#### 4.G. Interim Reclamation and Test Plots

The following three tests are suggested to be conducted in test plots completed during the TSF's operational life:

- 1. Test capillary rise by depositing slimes and allowing them to dry. Samples will be collected annually to determine if salts will migrate and accumulate at the surface.
- Test various organic amendments, fertilizer rates, mulches and species to determine an optimum mix for reclamation. Tests would be performed on samples of wet slimes (to simulate conditions at closure) and drained slimes and sands.
- 3 Samples of plant tissue will be collected and analyzed for copper and molybdenum concentrations to determine the potential for molybdenosis.

The tailings can be applied to the test area hydraulically. This will eliminate the need to mechanically transport material which has been deposited in the TSF.

# 4.H. Post Reclamation Maintenance and Monitoring

There are no specific reclamation success criteria in the BLM regulations. DOGM regulations (Rule 6474-111.13) require that revegetation achieve 70 percent of the premining vegetative ground cover and survive three growing seasons. If the pre-mining ground cover is unknown, the ground cover of an adjacent undisturbed area that is representative of the pre-mining ground cover can be used as a standard. Monitoring will begin the first fall after seeding is completed. Monitoring will include evaluating:

- \* erosion control
- \* noxious weed control
- vegetation success

Vegetation success monitoring will begin the first year following seeding. Monitoring for the first and second years will consist of a visual inspection of the seeded areas to identify areas where vegetation has not established. Any bare areas larger than 100 ft x 100 ft identified will be reseeded and/or amended as necessary.

Quantitative vegetation success monitoring will be estimated along a series of transects designed to representatively and evenly sample the tailings surface and an adjacent representative undisturbed area. Transects will be added until a statistically adequate sample size is determined. Sample adequacy will be determined using species-area curves. Annual monitoring will continue until results indicate vegetative cover on the tailings is 70 percent of the reference area. If the standard has not been achieved within 8 years after final seeding, SF Phosphates will request that the DOOM issue a determination that the revegetation work has been satisfactorily completed within practical limits.

Erosion control monitoring will be performed coincident with vegetation success monitoring and following significant precipitation events. Significant precipitation events are defined as at least one-half the intensity of the 10-year, 24-hour storm event.

Soil stability will be estimated for all reclaimed areas using the qualitative descriptors listed in Table 13 (NRC 1994). A qualified technician will observe each reclaimed area and assign one of the listed qualitative descriptors. The monitoring results will be used to aid in determining the cause of any failures which are encountered and to locate problem areas before erosion becomes widespread enough to affect water quality.

Any reclaimed area larger that 100 feet by 100 feet receiving an evaluation score (Table 13) of Class 3 or lower which persists more that 1 year will be investigated. Areas receiving a score of Class 2 or lower will receive treatment to correct the erosion immediately. If the vegetative cover, riprap, or other erosion control measure is found to be inadequate, the measures will be redone. Any obvious reasons for the failure will be noted and rectified. Climatic data for the time periods involved will also be considered while making a determination of the cause of failure.

Noxious weed monitoring will be performed during revegetation success monitoring. Prior to reclamation, a list of noxious weeds will be obtained from the local noxious weed control authority, if available. If noxious weeds are observed, appropriate measures will be taken to eradicate them. Species of concern, include:

- \* cheat grass (Anasantha tinctorum)
- \* tamarisk (Tamarix spp.)
- \* Russian olive (el.aeagnus angustifolia)

Noxious weed monitoring will continue until revegetation success criteria have been met.

SF PHOSPHATES
PLAN OF OPERATIONS.

SEPTEMBER 17, 1998

1201BS 1ACRC 1=,000H 1B/FTZ = 0.45 1B/1000FT?

## 5.0 STATEMENT OF RECLAMATION AND CLOSURE RESPONSIBILITY

SF Phosphates accepts responsibility for the reclamation and hazard abatement of the surface area affected by the mining and milling operations. Methods to be used to ensure successful reclamation were summarized in Section 4. These methods will include Best Management Practices and other techniques approved by regulatory agencies.

### 6.0 RECLAMATION COSTS

The following information provides costs and supporting documentation that will be the basis for establishing a reclamation bond as required by the BLM's bonding policy and the Utah Division of Oil, Gas and Mining (DOGM). These calculations are based upon the area on land (23.8 acres) administered by the BLM. They are estimated using the Means Heavy Construction Cost Data, 12th Annual Edition. Since specific details of the reclamation will be determined as the operation progresses, for example the exact seed mix, these calculations are intended to be very conservative.

Means 029 308 4600 - Slope mix,6#/M.S.F. Hydroseeding with mulch and fertilizer - \$2,026 /acre

23.8 acres x \$2,026 = \$48,220 + 10% (Administration fees) = \$53,040

The proposed reclamation cost is \$53,040. Administrative fees are calculated at 10% as required by the BLM. Administrative costs include administration, engineering specifications and plans, permits, utilities, insurance, legal fees, and travel costs.

Based upon the Memorandum of Understanding (MOU) between BLM and DOGM, it is desired that one bond for the entire operation be placed with DOGM. Specific language for the amount calculated herein to protect the public lands would be included.

## 7.0 PUBLIC SAFETY

The operating and reclamation procedures outlined in this Plan of Operations are designed to insure a safe, stable environment that provides for the highest degree of public safety. All safety procedures implemented will be in accordance with the requirements by the Utah Division of Oil, Gas and Mining.

The proposed tailings dam expansion has been designed with adequate freeboard to contain the runoff from the upland watershed during a probable maximum precipitation event (PMP) of 8.9 inches. Total PMP runoff from the watershed was calculated to be 1,986-acre feet which would be safely contained within the impoundment at all times with no discharge. A minimum additional freeboard of 3 feet would be maintained at all times for wave action and embankment settlement.

During operation, the tailings dam, reclaim water pumping, seepage reclaim, and tailings discharge systems are visually inspected each shift and any obvious irregularities are noted and responded to as required.

The current embankment piezometric monitoring for the existing tailings dam consists of three standpipe piezometers that are monitored monthly. These will be extended up through the future raises so this monitoring can continue for the duration of impoundment operations.

For the new raises, piezometers are proposed to be placed in the cycloned sand beach to monitor the piezometric levels within the sands. They will be monitored monthly during impoundment operations

Five settlement monuments are proposed to be constructed on the downstream crest of the embankment at the completion of each raise. The settlement monuments will be steel plates placed in concrete which will be surveyed every 6 months during the TSF life to provide information on embankment settlement.

## 8.0 BIBLIOGRAPHY

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## Millsite Claims Summary

Mill	Site	
Clair	m Nam	e

TB 1
TB 3-7
TB 10-13
TB 16-19
TB 23-27
TB 32-35
TB 43-46
TB 54-57
TB 79
TB 86

TC 1-77

B 1-12 B 12A B 13-42 B 44-63 B 66-279

SF 1-9 SF 9a SF 10-16 BLM Serial Number

UMC 60082 UMC 60084-60088 UMC 60091-60094 UMC 60097-60100 UMC 60104-60108 UMC 60113-60116 UMC 60124-60127 UMC 60135-60138 UMC 60160 UMC 60167

UMC 60266-60342

UMC361669-680 UMC361681 UMC361682-711 UMC361713-732 UMC361735-948 APPENDIX B

TABLE 7

## NUTRIENT ANALYSES LABORATORY RESULTS SF PHOSPHATES TAILINGS

			Lox	Location			Critical
	Tails Sand #1	Samd #2	Sand #3	Tails Slime #1	Slime #2	Slime #3	Value
Hd	7.2	7.0	7.1	7.2	7.2	7.2	<5.0 or >8.5
EC (mmhos/cm @ 25° C)	1.79	2.63	2.20	2.65	2.71	2.62	<b>&amp;</b>
Saturation (%)	34.9	30.3	31.9	37.3	37.0	34.6	<25 or > 80
Calcium (meq/l)	14.5	24.5	23.2	24.2	24.4	23.2	1
Magnesium (meq/l)	5.33	8.67	3.90	8.31	8.88	8.58	i
Sodium (meq/l)	1.20	1.27	0.52	1.75	1.87	1.7	1
SAR	0.38	0.31	0.14	0.43	0.46	4.0	<b>01 ^</b>
Sand (%)	84.0	81.0	84.0	26.0	20.0	28.0	1
Silt (%)	8.0	10.0	9.0	64.0	71.0	61.0	i
Clay (%)	8.0	0.6	10.0	10.0	9.0	11.0	i
Texture	loamy sand	loamy sand	loamy sand	silt loam	silt loam	silt loam	1
Organic Matter (%)	8.0	6.0	0.0	1.2	1.3	1.2	⊽
CEC (meq/100 g)	5.28	4.56	6.12	7.00	6.22	6.54	-
Plant Available							
P (ppm)	3.80	2.54	2.20	14.8	12.5	13.5	<i>L&gt;</i>
K (ppm)	0.46	87.0	0.89	82.0	84.0	82.0	<120
Nitrate-Nitrogen (ppm)	1.24	1.02	0.92	0.74	0.50	0.48	< 10
Copper (ppm)	0.24	0.34	0.32	0.46	0.46	0.46	1
Lead (ppm)	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	ł
Arsenic (ppm)	4.0	0.36	0.21	0.45	4.0	0.46	i
Boron (ppm)	0.17	0.24	0.13	0.20	0.22	0.23	<0.5 or >5
Selenium (ppm)	0.02	0.02	<0.02	0.02	0.02	0.02	>0.1
Molybdenum (ppm)	99:0	0.71	0.73	99.0	0.63	0.71	0.5 - 1.0
Iron (ppm)	13.2	16.4	9.0	50.4	8.4	54.0	1
Manganese (ppm)	09:0	1.04	1.16	2.18	1.88	1.98	ı
Zinc (ppm)	0.46	1.48	5.10	0.64	0.60	0.62	<1.0
Total Metals				234616,111			
Total Boron (ppm)	27.2	18.7	21.8	19.4	14.9	14.0	1
Total Arsenic (ppm)	19.4	27.0	26.1	18.1	18.9	19.1	20 - 20
Total Copper (ppm)	13.8	50.6	18.3	19.4	18.4	19.5	60 - 120
Total Lead (ppm)	<0.01	<0.01	<0.01	<0.01	<0.01	7.49	100 - 400
Total Molybdenum (ppm)	5.43	5.40	5.94	4.97	4.98	5.99	2 - 10
Total Selenium (ppm)	3.29	6.38	5.60	5.52	5.55	5.68	5 - 10
Total [ron (ppm)	9,930	15,100	14,500	9,440	9,720	10,300	i
Total Manganese (ppm)	83.0	81.5	87.1	174	172	168	i
Total Zinc (ppm)	162	170	179	109	110	108	70 - 400
Total Kjeldahl (Nitrogen %)	0.01	0.01	0.01	0.01	0.01	0.0	i

Notes:

Critical values were determined from a review of the available literature and represent values above Critical values we essent to a person which toxicity may result and below which deficiencies many result. However, these levels can vary significantly as a function of plant species, soil pH, texture, and may other features.

**Golder Associates** 

TABLE 8

## ACID-BASE ACCOUNTING RESULTS SF PHOSPHATES TAILINGS

Location   Location   Location   [ ]   Sand #3   Tails Slimi	12.1 12.2 13.8	1.89 1.73 1.22	59.0 54.0 38.1		65.5 73.6 97.5
#Tails Sand#1	Carbonate % 12.4	Fotal Sulfur % 0.93	T.S. AB t/1000t 29.1	Neut. Pot. t/1000t 127	T.S. ABP t/1000t 98.0

Note: T.S. = Total Sulfur

AB-Acid Base

Neutr. Pot. = Neutralization Potential

ABP=Acid Base Potential=Neut. Pot.-T.S. AB

TABLE 9

POTENTIAL RECLAMATION SPECIES SLIMES NURSE CROP

Scientific Name	Common Name				
Contract Con	Grass				
Agropyron cristatum	crested wheatgrass				
Alopecurus arundinaceus	creeping meadow foxtail				
Bromus biebersteinii	meadow brome				
Dactylis glomerata	orchardgrass				
Elymus trachycaulus	slender wheatgrass				
Elytrigia intermedia	pubescent wheatgrass				
Elytrigia pontica	tall wheatgrass				
Festuca arundinacea	tall fescue				
Muhlenbergia wrightii	spike muhly				
Pascopyrum smithii	western wheatgrass				
Phalaris arundinacea	reed canarygrass				
Psathyrostachys juncea	Russian wildrye				
Pseudoreogneria spicata inermis	beardless wheatgrass				
Stipa viridula	green needlegrass				
•	Forb				
Astragalus cicer	cicer milkvetch				
Coronilla varia	crownvetch				
Erodium circutarium	alfileria				
Lotus corniculatus	birdsfoot trefoil				
Medicago sativa	alfalfa				
Melilotus alba	white sweetclover yellow sweetclover				
Melilotus officinalis					
Onobrychis viciafolia	sainfoin				
Penstemon strictus	Rocky Mountain penstemon				
Sphaeralea coccinea	scarlet globemallow				
Vicia americana	American vetch				

TABLE 10
POTENTIAL RECLAMATION SPECIES FINAL COVER-SLIMES

Scientific Name	Common Name
	Grass
Agropyron cristatum	crested wheatgrass
Agropyron desertorum	standard crested wheatgrass
Agropyron Riparium	streambank wheatgrass
Athentherum hymenoides	Indian ricegrass
Elymus lanceolatus	thickspike wheatgrass
Hilaria jamesii	galleta
Pascopyrum smithii	western wheatgrass
Phalaris arundinacea	reed canarygrass
Psathyrostachys juncea	Russian wildrye
Sporobolus airoides	alkali sacaton
Sporobolus cryptandrus	sand dropseed
	Forb
Clematis ligusticifolia	virginsbower
Erodium cicutarium	alfileria
Kochia prostrata	prostrate summer cypress
Melilotus alba	white sweetclover
Melilotus officinalis	yellow sweetclover
Sphaeralcea coccinea	scarlet globemallow
	Shrub
Artemisia arbuscula nova	black sagebrush
Artemisia cana	silver sagebrush
Artemisia tridentata	big sagebrush
Atriplex canescens	fourwing saltbush
Atriplex nuttallii	Nuttall saltbush
Atriplex polycarpa	desert saltbush
Caragana arborescens	Siberian peashrub
Chrysothamnus nauseosus	rubber rabbitbrush
Cowania mexicana	cliffrose
Eurotia lanata	winterfat
Juniperus osteosperma	Utah juniper
Purshia tridentata	antelope bitterbrush
Rhus trilobata	skunkbush sumac

TABLE 11
POTENTIAL RECLAMATION SPECIES SAND BEACH

Scientific Name	Common Name			
	Grass			
Achnetherum hymenoides	Indian ricegrass			
Agropyron fragile	Siberian wheatgrass			
Agropyon riparium	streambank wheatgrass			
Elymus trachycaulus	pubescent wheatgrass			
Leymus racemosus	mammoth wildrye			
Sporobolus airoides	alkali sacaton			
Sporobolus contractus	spike dropseed			
Sporobolus cryptandrus	sand dropseed needle and thread			
Stipa comata				
	Shrub			
Atriplex canescens	fourwing saltbrush			
Atriplex nuttallii	Nuttall saltbush desert saltbrush Siberian peashrub rubber rabbitbrush			
Atriplex polycarpa				
Caragana arborescens				
Chrysothamnus nauseosus				
Cowania mexicana	cliffrose			
Ephedra viridis	green ephedra			
Juniperus osteosperma	Utah juniper			

## TABLE 12

## POTENTIAL RECLAMATION SPECIES POND AREA

Scientific Name	Common Name		
	Grass		
Deschampsia caespitosa	tufted hairgrass		
Distichlis stricta	inland saltgrass		
Juncus spp.	rush		
Muhlenbergia asperifolia	alkali muhly		
Poa palustris	fowl bluegrass		
Scirpus americanus	american bulrush		
Typha latifolia	common cattail		
	Forb		
Dodecatheon pulchellum	shooting star		
Iris missouriensis	Rocky Mountain iris		
Mertensia cilata	mountain bluebells		
Mimulus spp.	monkey flower		
Oenothera hookeri	Hooker evening prinrose		
Potentilla anserina	silverweed cinquefoil		
Ranunculus repens	creeping buttercup		
•	Shrubs/Trees		
Acer glabrum	mountain maple		
Acer grandidentata	big tooth maple		
Acer negundo	boxelder maple		
Alnus tenuifolia	thinleaf alder redosier dogwood quaking aspen		
Cornus stolonifera			
Populus tremuloides			
Prunus emarginata	bitter cherry		
Prunus virginiana	chokecherry		
Ribes aureum	golden currant		
Salix bebbiana	bebb willow		
Salix exigua	coyote willow		
Sambucus coerulea	blueberry elder		
Shepherdia argentea	silver buffaloberry		

# QUALITATIVE DESCRIPTORS OF SOIL SURFACE STATUS

Characteristic	Class 1	Class 2	Class 3	Class 4	Class 5
Soil movement	Subsoil exposed over much of area; may have embryonic dunes and wind-scoured depressions	Soil and debris deposited against minor obstructions	Moderate movement of soil is visible and recent; slight terracing	Some movement of soil particles	No visual evidence of movement
Surface rock and/or litter	Very little remaining (use care on low-productivity sites); if present, surface rock or fragments exhibit some movement and accumulation of smaller fragments behind obstacles	Extreme movement is apparent; large and numerous deposits against obstacle; if present, surface rock or fragments exhibit some movement and accumulation of smaller fragments behind obstacles	Moderate movement is apparent and fragments are deposited against obstacles; if present, fragments have a poorly developed distribution pattern	May show slight movement; if present, coarse fragments have a truncated appearance or spotty distribution caused by wind or water	Accumulation in place; if present, the distribution of fragments shows no movement caused by wind or water
Pedestaling	Most rocks and plants are pedestaled and roots are exposed	Rocks and plants on pedestals are generally evident; plant roots are exposed	Small rock and plant pedestals occurring in flow patterns	Slight pedestaling, in flow patterns	No visual evidence of pedestaling
Flow patterns	Flow patterns are numerous and readily noticeable; may have large barren fan deposits	Flow patterns contain silt, sand deposits, and alluvial fans	Well defined small, and few with intermittent deposits	Deposition of particles may be in evidence	No visual evidence of flow patterns
Rills and gullies	May be present at depths of 8 to 15 cm (3 to 6 inches) and at intervals of less than 13 cm (15 inches); sharply incised gullies cover most of the area, and 50 percent are actively eroding	Rills at depths of 1 to 15 cm (0.5 to 6 inches) occur in exposed areas at intervals of 150 cm (5 feet); gullies are numerous and well developed, with active erosion along 10 to 50 percent of their lengths or a few well-developed gullies with active erosion along more than 50 percent of their lengths.	Rills at depths less than 15 cm occur in exposed places at intervals of less than 300 cm (10 ft); gullies present, with active erosion along less than 10 percent of their length; some vegetation may be present	Some rills in evidence at infrequent intervals of over 300 cm (10 feet); evidence of gullies that show little bed or slope erosion; some vegetation is present on slopes	No visual evidence of rills; may be present in stable condition; vegetation on channel bed and side slopes

SOURCE: Adapted from U.S. Department of the Interior, Bureau of Land Management. 1973 Determination of Erosion Condition Class, Form 7310-12. May. Washington, D.C.: U.S. Department of the Interior

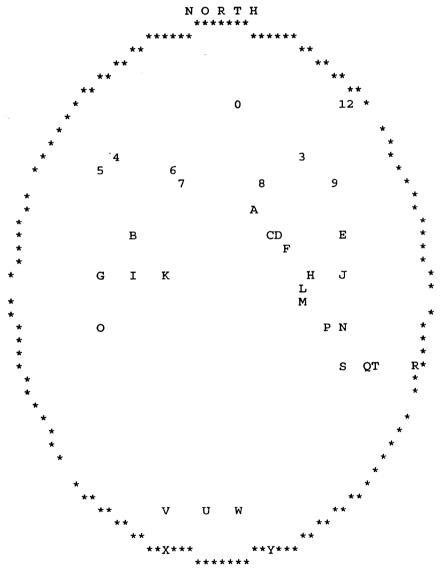
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UTAH DIVISION OF WATER RIGHTS
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PLOT SHOWS LOCATION OF 45 POINTS OF D

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PLOT SCALE IS APPROXIMATELY 1 INCH = 3000



UTAH DIVISION OF WATER RIGHTS
NWPLAT POINT OF DIVERSION LOCATION P

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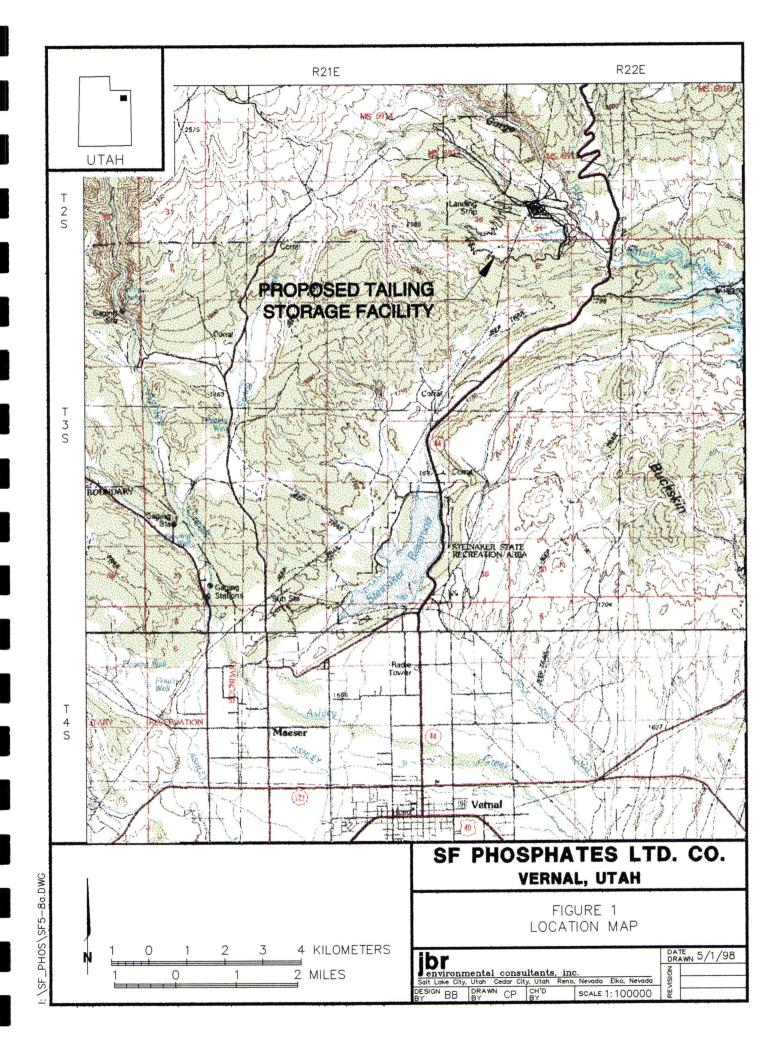
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		USA Bureau of	Land Management	P.O. Box 45155
1	45 2685	WATER USE(S):	STOCKWATERING	East Cottonwood Canyon Stream
		SF Phosphates	Limited Company	9401 North Highway 191
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		SF Phosphates	IRRIGATION DOMES	9401 North Highway 191
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		SF Phosphates	Limited Company	9401 North Highway 191
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		SF Phosphates	IRRIGATION DOMES	9401 North Highway 191
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		SF Phosphates	Limited Company	9401 North Highway 191
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		SF Phospahtes	DOMESTIC OTHER Limited Company	9401 North Highway 191
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		WATER USE(S): SF Phosphates	DOMESTIC OTHER Limited Company	9401 North Highway 191

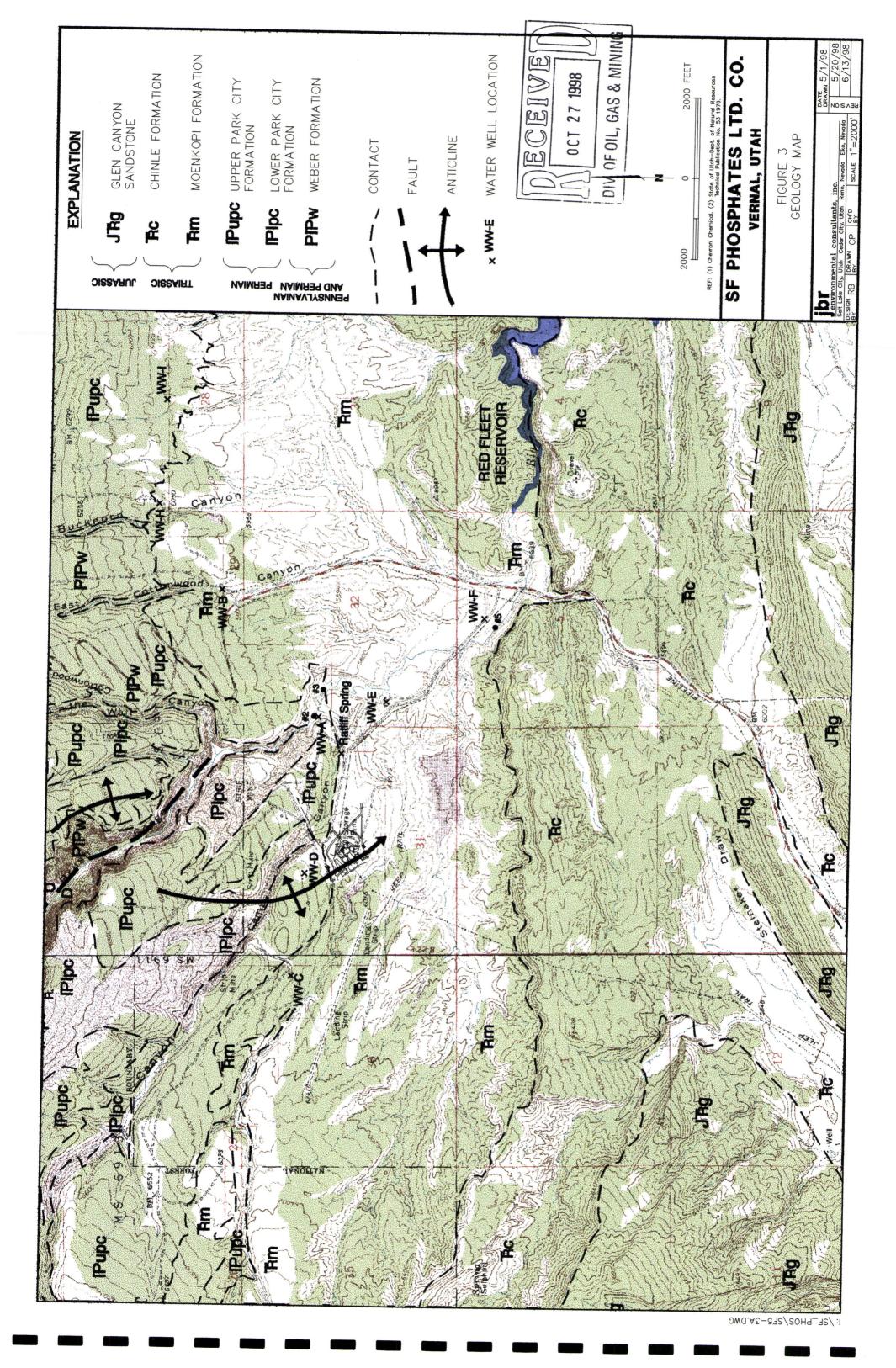
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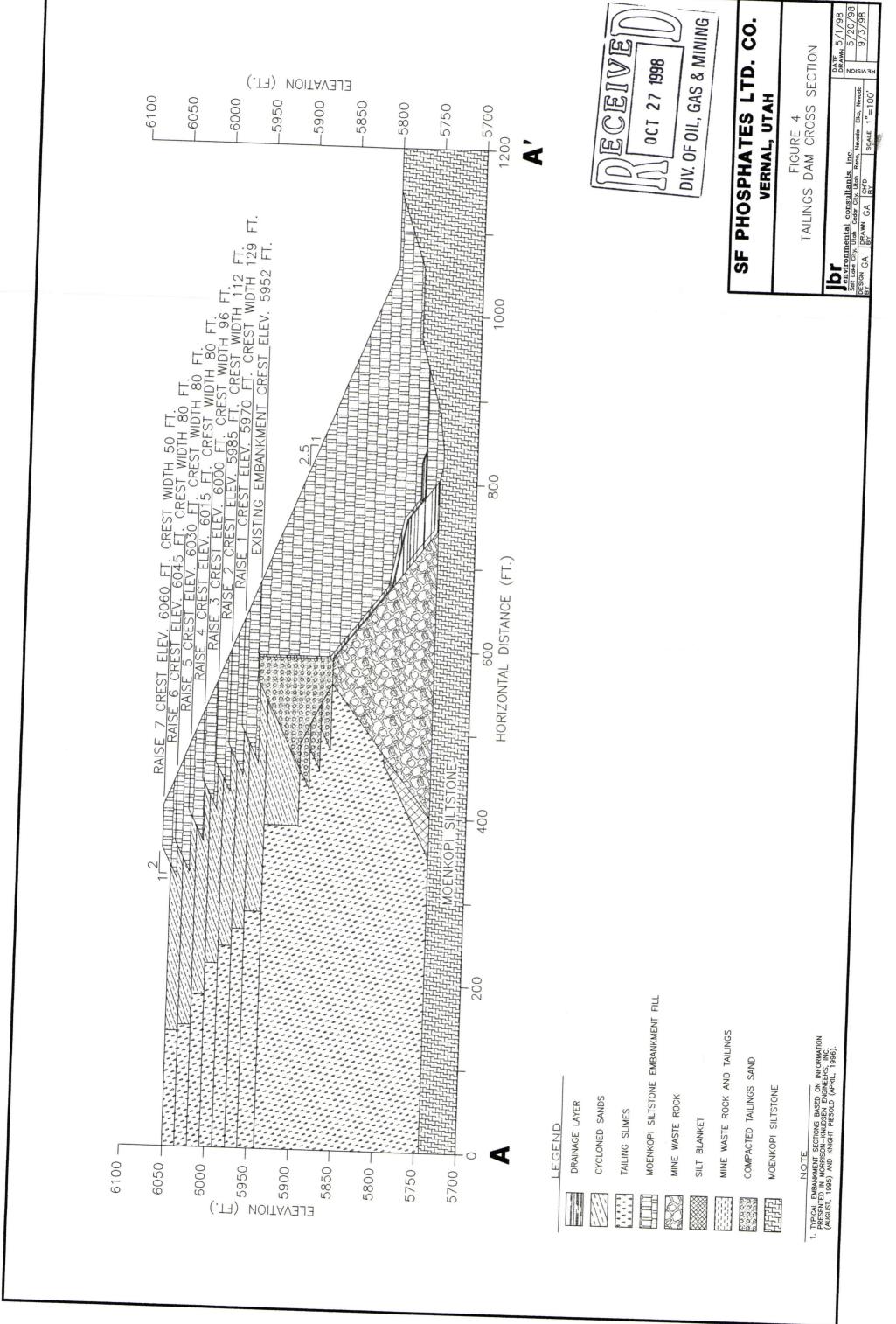
UTAH DIVISION OF WATER RIGHTS POINT OF DIVERSION LOCATION P NWPLAT

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G	45 1817	.0000	.00	Tributary t	to Cottontail Draw		
		WATER USE(S): State of Utah	STOCKWATERING School & Institu	utional Tru	675 East 500 South, 5	5th	Floo
н	45 1814	.0000 WATER HER(S):	.00	Cottontail	Draw		
					9401 North Highway 19	<b>}</b> 1	
I	45 1813	WATER HISE(S) .	.00 STOCKWATERING				
			Land Management				
Ι	45 1818	WATER USE(S):	.00 STOCKWATERING Land Management				
J	45 3008	.0000	.00		to Big Brush Creek		
		WATER USE(S): USA Bureau of	STOCKWATERING Land Management		P.O. Box 45155		
J	45 1811	WATED HER (C) .	STOCKWATERING		nwood Canyon Stream		
		USA Bureau of	Land Management				
K	45 1818	.0000 WATER USE(S):	.00 STOCKWATERING	Trib. to Co	ottontail Draw		

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P.O. Box 45155
          USA Bureau of Land Management
                                  .00 Cottontail Draw
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           WATER USE(S): STOCKWATERING
                                              9401 North Highway 191
          SF Phosphates Limited Company
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MAP WATER QUANTITY SOURCE DESCRIPTION OF WELL INFO PO
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          Humphreys Phosphate Co.
                                .00 Big Brush Creek
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           WATER USE(S): STOCKWATERING
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           SF Phosphates Limited Company
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           WATER USE(S): STOCKWATERING
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          SF Phosphates Limited Company
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           USA Bureau of Land Management
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 X 45 957
           WATER USE(S): STOCKWATERING
                                                2290 South Orchard Drive
           Calder, Sydney
                                  .00 Trib. to Big Brush Creek
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 Y 45 1836
           WATER USE(S): STOCKWATERING
           USA Bureau of Land Management P.O. Box 45155
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